

# **APPENDIX H1**

## *Drainage Study*



**TENTATIVE MAP DRAINAGE STUDY  
For  
OTAY RANCH PORTION OF VILLAGE 4**

City of Chula Vista, California

Prepared for:  
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August 3, 2016

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increases will need to be considered in the projects design and addressed in this study. In addition, the proposed basin will also serve as a water quality and flow control (hydromodification) treatment facility for the developed portions of the site. All impervious areas constructed throughout the site will need to route their 85<sup>th</sup> percentile runoff through the 'water quality' basin. The proposed basin location is south of Main Street at the western edge of the development.

In Existing condition, the Village 4 South site generally flows in a northwesterly direction towards a tributary of Wolf Canyon at which time runoff will then travel west then south towards the Otay River. Development of the site will cut portions of land located at the higher elevations. Runoff will be collected within the proposed storm drain system which will eventually outlet into Wolf Canyon. Per the Flood Insurance Rate Map No. 06073C2178, the site lies outside the FEMA floodplain boundary. Therefore, a Letter of Map Revision is not required. See Exhibit 3 for an overlay of the site on Flood Insurance Rate Map which also includes the Savage Dam inundation flood line.

The MSCP Open Space Preserve is located along the site northern and western boundaries. With exceptions relative to sewer line and storm drain routing, the development of Otay Ranch Village 4 South, as proposed in the TM, will not encroach into the MSCP area and will have an assigned easement through the preserve. Since this project is located adjacent to a Preserve area, it will adhere to Section 7.5.2 of the City's *MSCP Subarea Adjacency Guidelines* pertaining to drainage and water quality.

Per the City of Chula Vista drainage criteria, the Modified Rational Method should be used to determine peak design flow rates when the contributing drainage area is less than 1.0-square mile. Since the total watershed area discharging from the Otay Ranch Village 3 site is less than 1.0-square mile, the AES-2010 computer software was used to model the runoff response per the Modified Rational Method.

Methodology used for the computation of design rainfall events, runoff coefficients, and rainfall intensity values are consistent with criteria set forth in the most current "San Diego County Hydrology Manual" and the "City of Chula Vista Subdivision Manual". A detailed explanation of methodology and model development used for this analysis is listed in Chapter 2 of this report.

## **1.2 Summary of Pre-Developed Conditions**

The topography for existing Village 4 South site is such that its runoff drains in a northwesterly direction towards a tributary of Wolf Canyon and subsequently to Wolf Canyon and the Otay River. The watershed which drains through the site has an elevation high point of about 650 ft. MSL. Several finger canyons subdivide the drainage areas but not in any significant hydrologic manner. Refer to Exhibit 1, Existing Hydrology Map in Chapter 4 for watershed boundary associated with the project area. The watershed area delineated on the map was determined as a means of equally comparing the impact of the proposed development with its comparable existing condition at a point immediately downstream of the proposed site at Wolf Canyon.

Table 1 below summarizes the 50 and 100-year pre-development peak flows from the site in existing condition. A runoff coefficient of 0.60 was used for the existing tributary areas per the City of Chula Vista Subdivision Manual. These coefficients correspond to vegetated steep slopes.

**TABLE 1 - Summary of Pre-Developed Flows to the Wolf Canyon**

<b>Discharge Location</b>	<b>Drainage Area (ac)</b>	<b>50-Year Peak Flow (cfs)</b>	<b>100-Year Peak Flow (cfs)</b>
Wolf Canyon	201.4	266.21	295.29

Supporting calculations for the data presented in Table 1 are located in Chapter 3 of this report. The corresponding hydrology map is Exhibit 1 in Chapter 5.

## **1.3 Summary of Developed Conditions**

The Otay Ranch Village 3 Tentative Map will consist of single and multi-family residential dwelling units, roads for circulation, and open space areas. The extension of Main Street west from the Village 8 West project boundary is also included with this development as well as offsite sewer lines and stormwater facilities. The proposed 'water quality/HMP' basin will be located on the south side of Main Street and west of the developed portions of Village 4 South.

The extension of Main Street will be approximately 3,700 linear feet from the eastern boundary of the site where it connects to Village 8 West. Runoff from Village 8 West does not drain onto Village 4 South. Instead, inlets within Village 8 West collect and direct runoff north towards a proposed water treatment basin before discharging into the Wolf Canyon tributary located immediately north of Village 4 South. See Exhibit 2, Proposed Condition Hydrology Map in Chapter 4. Water Quality and flow control (HMP) treatment of onsite Main Street runoff will be performed with the Village 4 South basin. For water quality and hydromodification discussion and calculations, please reference the *Priority Development Project (PDP) Storm Water Quality Management Plan (SWQMP) for Otay Ranch Portion of*

*Village 4 Tentative Map* dated August 2016 prepared by Hunsaker & Associates San Diego Inc.

In general, runoff from the developed site will drain north towards Main Street. Inlets placed throughout the site will collect the runoff and the storm drain will convey it towards the Main Street storm drain system. This storm drain system will convey flows west and then south before it reaches the future location of the proposed bridge abutment. It will outlet into the proposed basin located south of Main Street. The basin will consist of a riser with a rim height set to allow required ponding of the 'water quality' treatment design volume per the requirements set forth by the SDRWQCB Order R9-2013-0001. The basin's base will consist of 18" of engineered fill, 24" of gravel, and a perforated subdrain.

Table 2 below summarizes the 50 and 100-year developed condition peak flows at the location of the Wolf Canyon discharge including the effect of detention from the proposed basin. The discharge point at Wolf Canyon is shown on Exhibit 2 in Chapter 5. Runoff coefficients assumed for the proposed roads, multi-family development and single family development are per the City of Chula Vista Subdivision Manual.

**TABLE 2 - Summary of Developed Flows to Otay River**

<b>Discharge Location</b>	<b>Drainage Area (ac)</b>	<b>50-Year Peak Flow (cfs)</b>	<b>100-Year Peak Flow (cfs)</b>
Wolf Canyon	203.09	259.32	292.50

Supporting calculations for the information presented in Table 2 is located in Chapter 3 and 4 of this report. The corresponding hydrology map is Exhibit 2 in Chapter 5.

The storm drain outlet into the Wolf Canyon will require the design of an appropriate outlet structure to dissipate flow velocities. The outlet structure selected will reduce velocities downstream so as to not create an erosive situation. Options available include, but are not limited to, APWA energy dissipating impact basins, (SDRSD) D-41 Concrete Energy Dissipators, and rip rap energy dissipation.

Landform grading has been incorporated to mimic existing conditions where the proposed grading ties into or daylight with the existing terrain. It is intended that the stormwater from the manufactured slopes will sheet flow and follow the existing drainage patterns.

**1.4 Results & Recommendations**

Table 3 summarizes the effects of site development at the receiving Otay River.

**TABLE 3 - Summary of Pre vs. Post-Developed Flows from Village 4 South**

Discharge Location	PRE-DEVELOPED		POST-DEVELOPED		DIFFERENCE	
	Drainage Area (ac)	100-Year Peak Flow (cfs)	Drainage Area (ac)	100-Year Peak Flow (cfs)	Area (ac)	100-Year Peak Flow (cfs)
Wolf Canyon	201.4	295.29	203.09	292.50	+1.69*	-2.79

\*-Increase in area is due to the basin area which was not included in the Existing Condition.

Development of Otay Ranch Village 4 South TM results in the net decrease of runoff discharged to Wolf Canyon of approximately 2.79 cfs when considering the effect of the proposed detention basin.

A comparison of the existing and proposed condition maps illustrates that there are finger canyons along the northern side of the site which show an area reduction, and thus flow reduction compared to the existing condition. Therefore, the potential for erosion has been greatly reduced immediately downstream of these finger canyons. Since the flows have been reduced for these subareas, existing flow velocities should not be exceeded once the site has been developed. Therefore, erosion is not expected at the downstream points of these subareas.

Erosion Control: The developer shall monitor any erosion at the project’s outfall at Wolf Canyon and, prior to the last building permit for the project, obtain approval for and complete any reconstructive work necessary to eliminate any existing erosion and prevent future erosion from occurring, all to the satisfaction of the Development Services Director.

Scour Analysis: Concurrent with all grading plan submittals, the applicant shall prepare a scour analysis for all structures within the 100-year flood hazard area. Additionally, all said structures shall be monitored until the last building permit for the project has been issued.

Summary:

- Drainage facilities within Village 4 South will be designed in accordance with the requirements of the Chula Vista Subdivision Manual, the San Diego County Hydrology Manual and the requirements of the San Diego Regional Water Quality Control Board.
- Development of the project site will not further degrade potential beneficial uses of downstream water bodies as designated by the Regional Water Quality Control Board, including water bodies listed on the Clean Water Section 303d list.
- Onsite and offsite drainage easements shall be provided to the satisfaction of the Director of Public Works.

## **References**

*City of Chula Vista Subdivision Manual; Engineering Department and Land Development; Section 3-200, March 13, 2012*

*San Diego County Hydrology Manual; County of San Diego Department of Public Works Flood Control Division, June 2003*

*Hydromodification Management Plan prepared for County of San Diego, California, March 2011*

*Priority Development Project (PDP) Storm Water Quality Management Plan (SWQMP) for Otay Ranch Portion of Village 4 Tentative Map prepared by Hunsaker and Associates, San Diego Inc., August 2016.*

*“Order No. R9-2013-0001, NPDES No. CAS0109266 – Waste Discharge Requirements for Discharges of Urban Runoff from the Municipal Separate Storm Sewer Systems (MS4s) Draining the Watersheds of the County of San Diego, the Incorporated Cities of San Diego County, San Diego Unified Port District and the San Diego County Regional Airport Authority”, California Regional Water Quality Control Board – San Diego Region.*

## CHAPTER 2 - METHODOLOGY

### 2.1 - Rational Method Model Development Summary

Computer Software Package – AES-2015

Design Storm – 50 for storm drain and 100-Year for detention and sump inlets

Land Use – Multi Family, Single Family, and Open Space

Soil Type - Hydrologic soil group D was assumed for all areas. Group D soils have very slow infiltration rates when thoroughly wetted. Consisting chiefly of clay soils with a high swelling potential, soils with a high permanent water table, soils with clay pan or clay layer at or near the surface, and shallow soils over nearly impervious materials, Group D soils have a very slow rate of water transmission.

Runoff Coefficient – In accordance with the City of Chula Vista Subdivision Manual, a runoff coefficient of 0.90 was used for fully paved areas, 0.75 for the Multi-Family Sites and dense residential, 0.65 for the Single-Family pads, 0.35 for proposed open space, and 0.30 for parks.

Method of Analysis – The Rational Method is the most widely used hydrologic model for estimating peak runoff rates. Applied to small urban and semi-urban areas with drainage areas less than 1.0 square mile, the Rational Method relates storm rainfall intensity, a runoff coefficient, and drainage area to peak runoff rate. This relationship is expressed by the equation:

Q = CIA, where:

Q = The peak runoff rate in cubic feet per second at the point of analysis.

C = A runoff coefficient representing the area - averaged ratio of runoff to rainfall intensity.

I = The time-averaged rainfall intensity in inches per hour corresponding to the time of concentration.

A = The drainage basin area in acres.

To perform a node-link study, the total watershed area is divided into subareas which discharge at designated nodes.



The procedure for the subarea summation model is as follows:

- (1) Subdivide the watershed into an initial subarea (generally 1 lot) and subsequent subareas, which are generally less than 10 acres in size. Assign upstream and downstream node numbers to each subarea.
- (2) Estimate an initial  $T_c$  by using the appropriate nomograph or overland flow velocity estimation.
- (3) Using the initial  $T_c$ , determine the corresponding values of  $I$ . Then  $Q = C I A$ .
- (4) Using  $Q$ , estimate the travel time between this node and the next by Manning's equation as applied to the particular channel or conduit linking the two nodes. Then, repeat the calculation for  $Q$  based on the revised intensity (which is a function of the revised time of concentration)

The nodes are joined together by links, which may be street gutter flows, drainage swales, drainage ditches, pipe flow, or various channel flows. The AES-2010 computer subarea menu is as follows:

#### SUBAREA HYDROLOGIC PROCESS

1. Confluence analysis at node.
2. Initial subarea analysis (including time of concentration calculation).
3. Pipeflow travel time (computer estimated).
4. Pipeflow travel time (user specified).
5. Trapezoidal channel travel time.
6. Street flow analysis through subarea.
7. User - specified information at node.
8. Addition of subarea runoff to main line.
9. V-gutter flow through area.
10. Copy main stream data to memory bank
11. Confluence main stream data with a memory bank
12. Clear a memory bank

At the confluence point of two or more basins, the following procedure is used to combine peak flow rates to account for differences in the basin's times of concentration. This adjustment is based on the assumption that each basin's hydrographs are triangular in shape.

- (1). If the collection streams have the same times of concentration, then the  $Q$  values are directly summed,

$$Q_p = Q_a + Q_b; T_p = T_a = T_b$$

(2). If the collection streams have different times of concentration, the smaller of the tributary Q values may be adjusted as follows:

- (i). The most frequent case is where the collection stream with the longer time of concentration has the larger Q. The smaller Q value is adjusted by the ratio of rainfall intensities.

$$Q_p = Q_a + Q_b (I_a/I_b); T_p = T_a$$

- (ii). In some cases, the collection stream with the shorter time of concentration has the larger Q. Then the smaller Q is adjusted by a ratio of the T values.

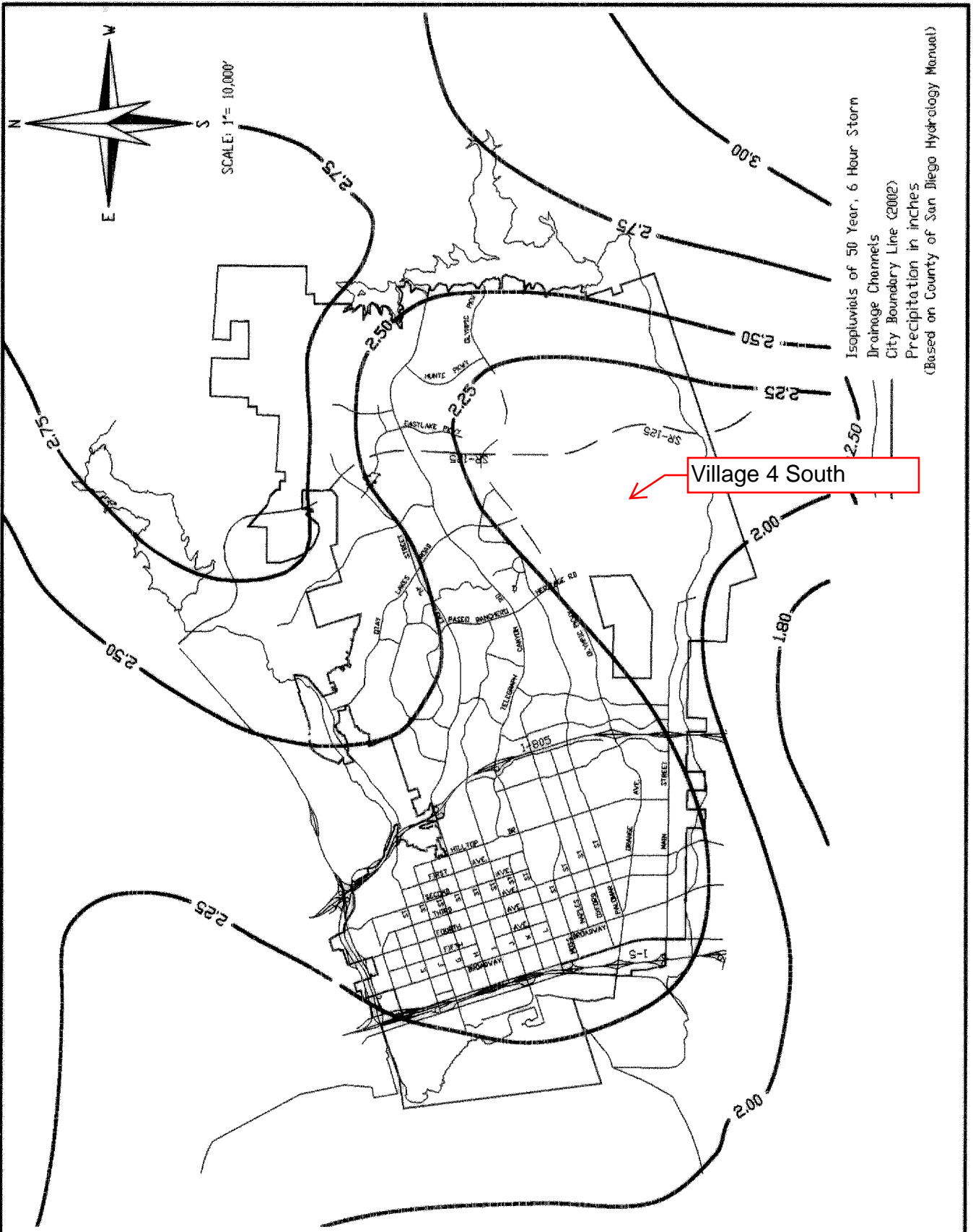
$$Q_p = Q_b + Q_a (T_b/T_a); T_p = T_b$$

## **CHAPTER 2**

### **METHODOLOGY & MODEL DEVELOPMENT**

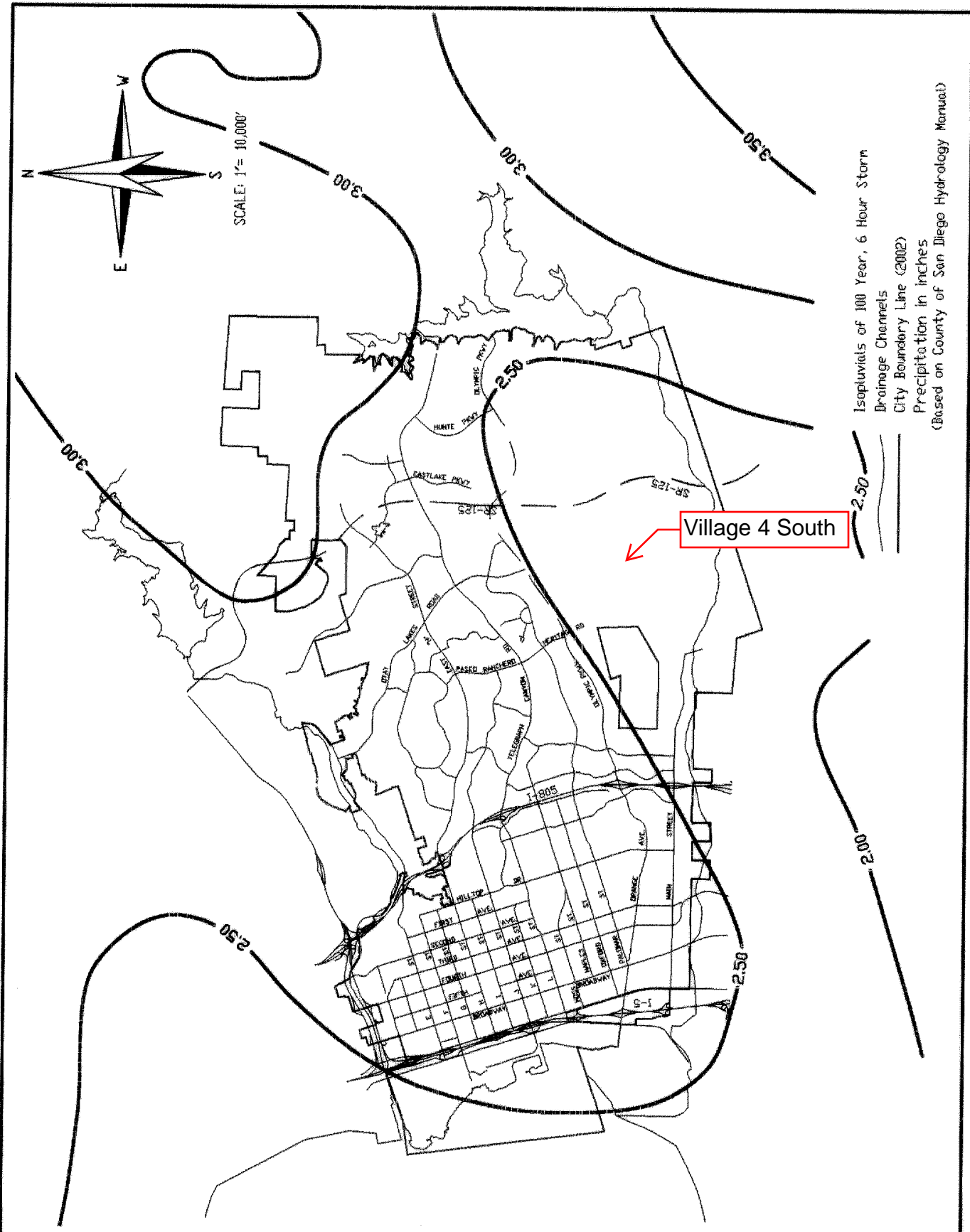
#### **2.2 – Design Rainfall Determination**

**50-Year, 6-Hour and 100-Year, 6-Hour Rainfall  
Isopluvial Maps from City of Chula Vista  
Design Standards – CVDS Storm Drain Design**



Revised:	Original approval date:	01-29-02
M.P.M 2-02	Redrawn By:	M.P.M Date: 01-29-02
	<i>Clifford Swanson</i>	
	CITY ENGINEER	Date: 11-7-02

CITY OF CHULA VISTA PUBLIC WORKS DEPARTMENT	
50 YEAR, 6 HOUR PRECIPITATION	CVD- DR04



Isopleths of 100 Year, 6 Hour Storm  
 Drainage Channels  
 City Boundary Line (2002)  
 Precipitation in inches  
 (Based on County of San Diego Hydrology Manual)

Revised: M.P.M 2-02	Original approval date: 01-29-02	CITY OF CHULA VISTA PUBLIC WORKS DEPARTMENT	
	Redrawn By: C.V.M.	Date: 01-29-02	100 YEAR, 6 HOUR PRECIPITATION
	<i>Bluffel Skramson</i>		CVD-DR05
	CITY ENGINEER	Date: 11-7-02	

## **CHAPTER 2**

### **METHODOLOGY & MODEL DEVELOPMENT**

#### **2.3 – Runoff Coefficient Determination**

3-203.3 **Rational and Modified Rational Methods**

(1) The rational method equation relates storm rainfall intensity (I), a selected runoff coefficient (C) and drainage area (A) to the peak runoff rate (Q):

$$Q = CIA \text{ (Empirical Units)}$$

where:

- Q = Peak runoff in cubic feet per second
- C = Runoff coefficient
- I = Intensity, inches per hours
- A = Drainage basin area in acres

Or

$$Q=0.278CIA \text{ (Metric Units)}$$

where:

- Q = Peak runoff in cubic meters per second
- C = Runoff coefficient
- I = Intensity in millimeters per second
- A = Drainage area in square kilometers

(2) Coefficient of Runoff: Consider probable development. Use highest number of the following values:

a)	Paved Surface	0.90
b)	Commercial Area	0.85
c)	Dense Residential (R2, R3)	0.75
d)	Normal Residential (R1)	0.65
e)	Suburban Property (RE)	0.55
f)	Barren Slopes Steep	0.80
g)	Barren Slopes Hilly	0.75
h)	" " Rolling	0.70
i)	" " Flat	0.65
j)	Vegetated Slopes Steep	0.60
k)	" " Hilly	0.55
l)	" " Rolling	0.50
m)	" " Flat	0.45
n)	Farm Land	0.35
o)	Parks, Golf Courses	0.30

NOTES: Steep = Steep, rugged terrain with average slopes generally above 30%.  
 Hilly = Hilly terrain with average slopes of 10% to 30%.  
 Rolling = Rolling terrain with average slopes of 5% to 10%.  
 Flat = Relatively flat land, with average slopes of 0% to 5%.  
 Composite = Where drainage areas are composed of parts having different runoff characteristics, a weighted coefficient for the total drainage area may be used.

## **CHAPTER 2**

### **METHODOLOGY & MODEL DEVELOPMENT**

#### **2.4 – Rainfall Intensity Determination**

**-Maximum Overland Flow Length & Initial Time of Concentration**

**-Urban Watershed Overland Time of Flow  
Nomograph**

**-Gutter & Roadway Discharge-Velocity Chart**

**- Manning's Equation Nomograph**

**-Intensity-Duration Design Chart**



Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

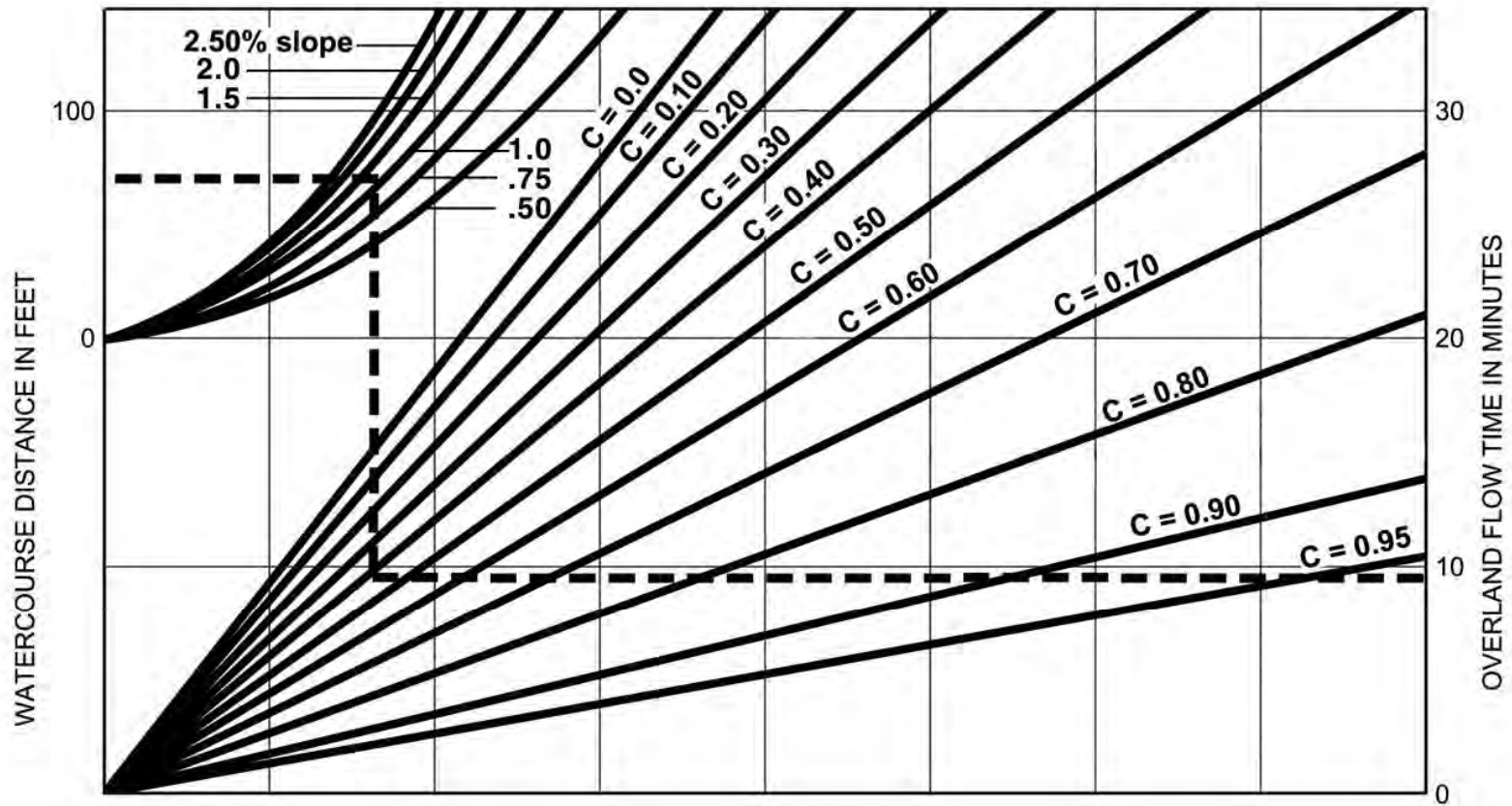
Table 3-2 provides limits of the length (Maximum Length ( $L_M$ )) of sheet flow to be used in hydrology studies. Initial  $T_i$  values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the “Regulating Agency” when submitted with a detailed study.

**Table 3-2**

**MAXIMUM OVERLAND FLOW LENGTH ( $L_M$ )  
 & INITIAL TIME OF CONCENTRATION ( $T_i$ )**

Element*	DU/ Acre	.5%		1%		2%		3%		5%		10%	
		$L_M$	$T_i$	$L_M$	$T_i$	$L_M$	$T_i$	$L_M$	$T_i$	$L_M$	$T_i$	$L_M$	$T_i$
Natural		50	13.2	70	12.5	85	10.9	100	10.3	100	8.7	100	6.9
LDR	1	50	12.2	70	11.5	85	10.0	100	9.5	100	8.0	100	6.4
LDR	2	50	11.3	70	10.5	85	9.2	100	8.8	100	7.4	100	5.8
LDR	2.9	50	10.7	70	10.0	85	8.8	95	8.1	100	7.0	100	5.6
MDR	4.3	50	10.2	70	9.6	80	8.1	95	7.8	100	6.7	100	5.3
MDR	7.3	50	9.2	65	8.4	80	7.4	95	7.0	100	6.0	100	4.8
MDR	10.9	50	8.7	65	7.9	80	6.9	90	6.4	100	5.7	100	4.5
MDR	14.5	50	8.2	65	7.4	80	6.5	90	6.0	100	5.4	100	4.3
HDR	24	50	6.7	65	6.1	75	5.1	90	4.9	95	4.3	100	3.5
HDR	43	50	5.3	65	4.7	75	4.0	85	3.8	95	3.4	100	2.7
N. Com		50	5.3	60	4.5	75	4.0	85	3.8	95	3.4	100	2.7
G. Com		50	4.7	60	4.1	75	3.6	85	3.4	90	2.9	100	2.4
O.P./Com		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
Limited I.		50	4.2	60	3.7	70	3.1	80	2.9	90	2.6	100	2.2
General I.		50	3.7	60	3.2	70	2.7	80	2.6	90	2.3	100	1.9

\*See Table 3-1 for more detailed description



EXAMPLE:

Given: Watercourse Distance (D) = 70 Feet  
 Slope (s) = 1.3%  
 Runoff Coefficient (C) = 0.41  
 Overland Flow Time (T) = 9.5 Minutes

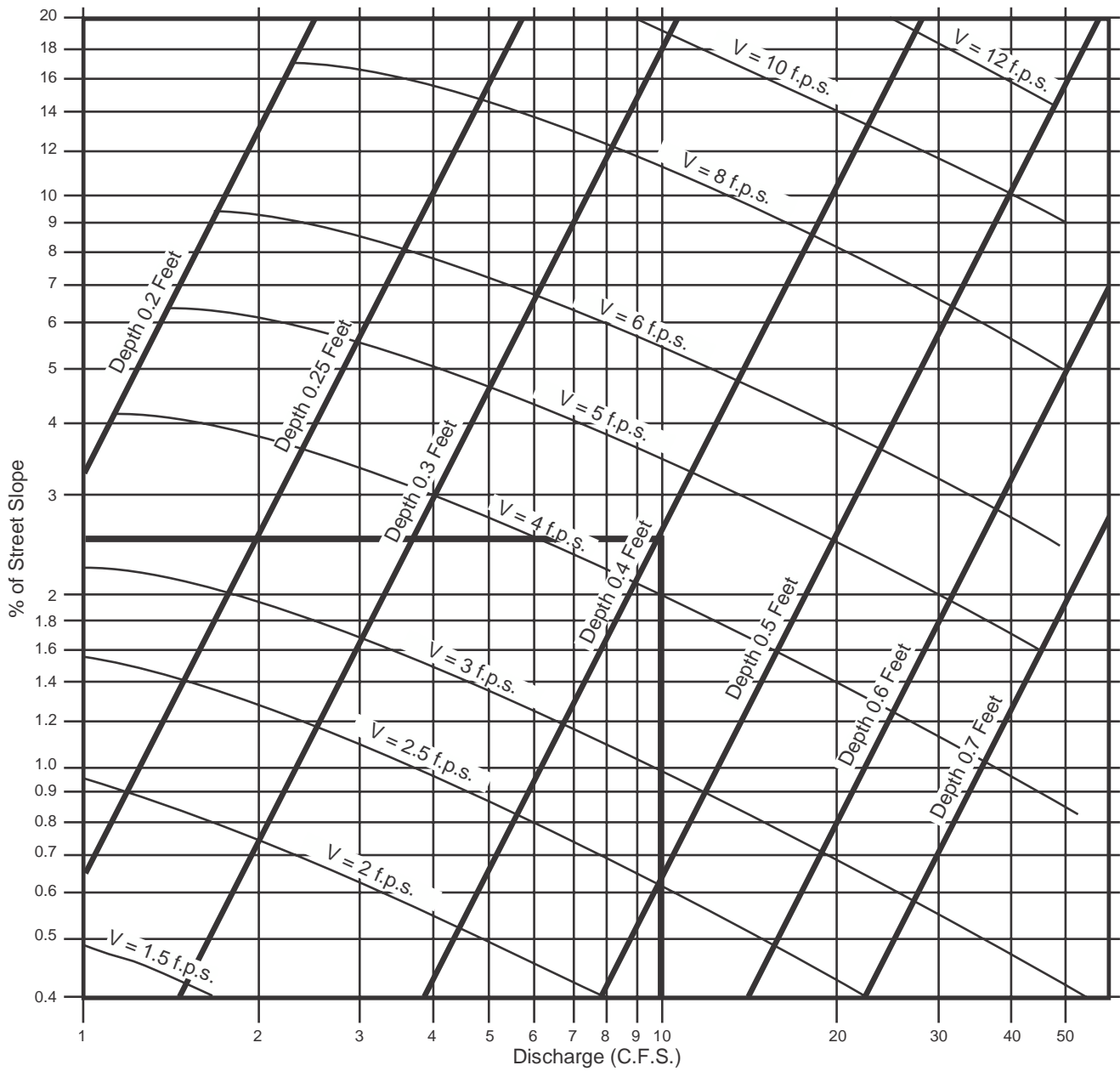
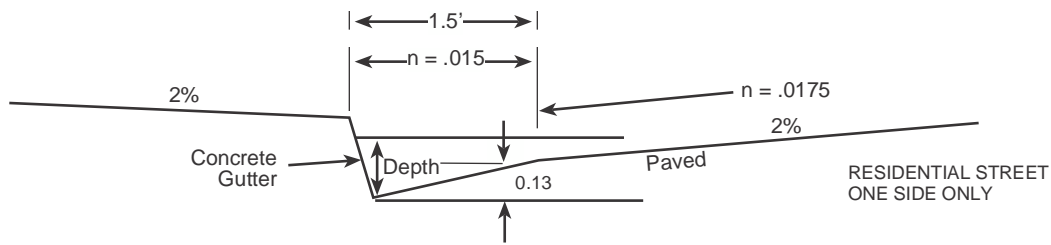
$$T = \frac{1.8 (1.1-C) \sqrt{D}}{\sqrt[3]{s}}$$

SOURCE: Airport Drainage, Federal Aviation Administration, 1965

Rational Formula - Overland Time of Flow Nomograph

FIGURE

3-3



**EXAMPLE:**  
 Given:  $Q = 10$   $S = 2.5\%$   
 Chart gives: Depth = 0.4, Velocity = 4.4 f.p.s.

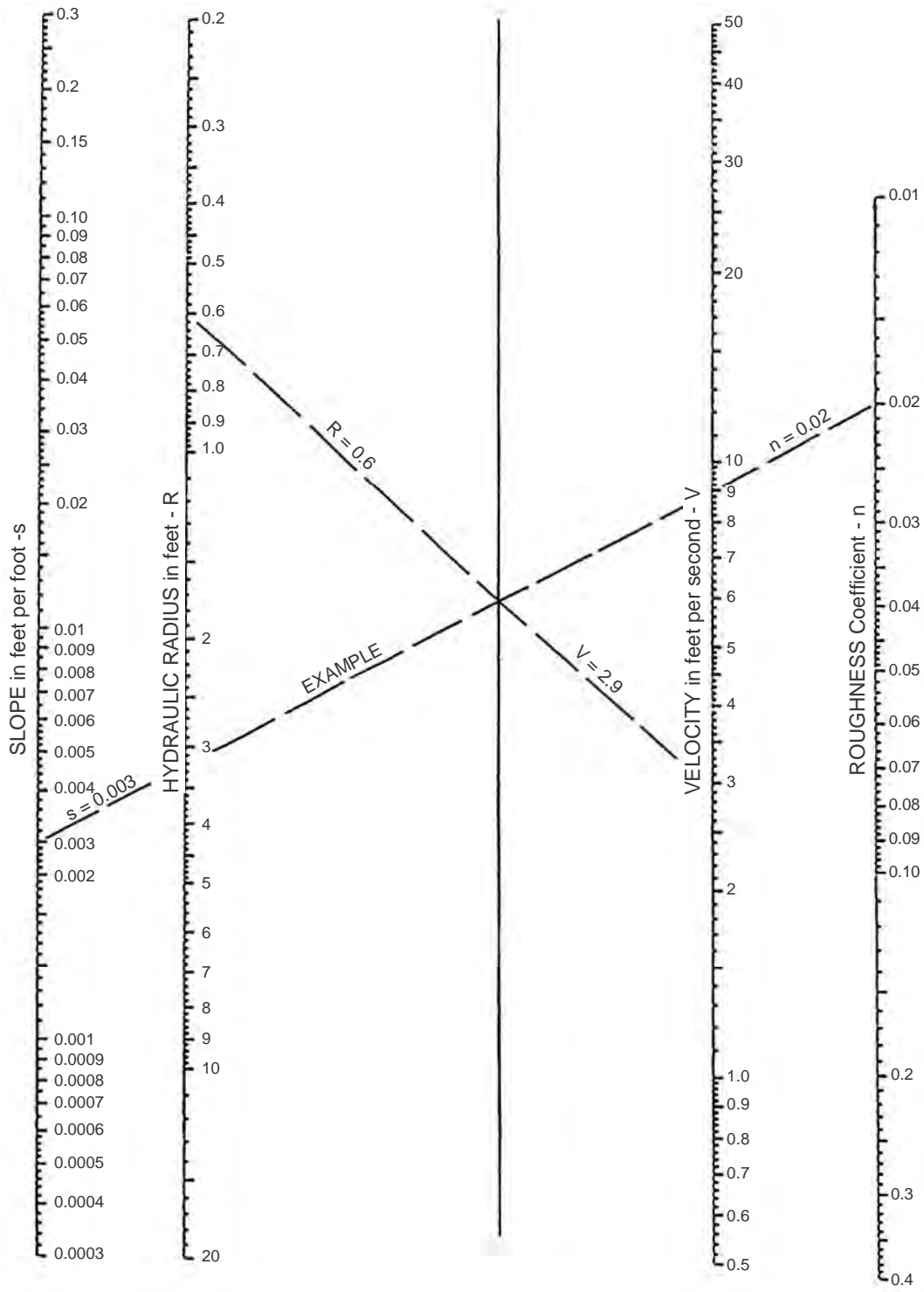
SOURCE: San Diego County Department of Special District Services Design Manual

Gutter and Roadway Discharge - Velocity Chart

FIGURE

3-6

$$\text{EQUATION: } V = \frac{1.49}{n} R^{2/3} s^{1/2}$$

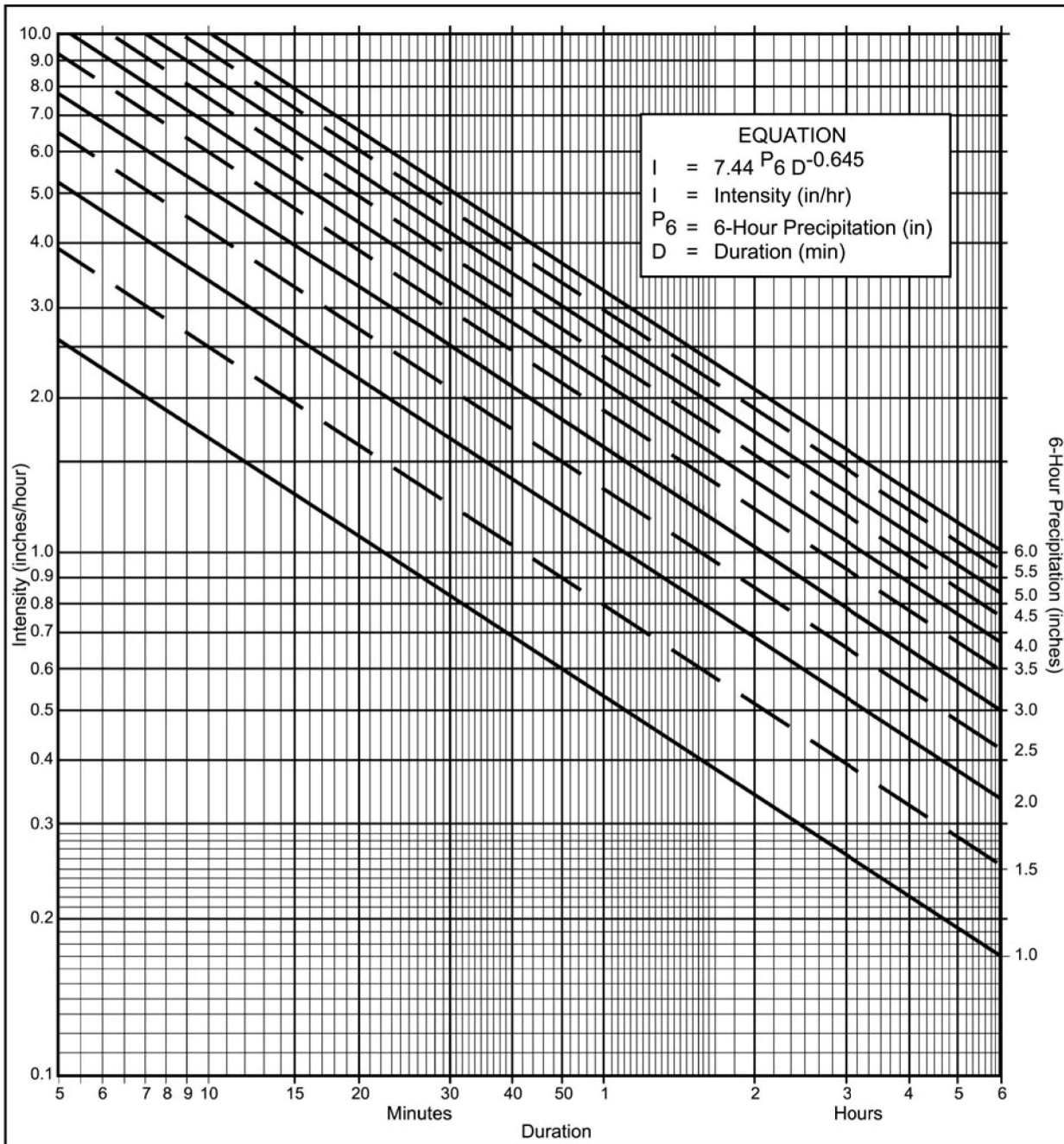


SOURCE: USDOT, FHWA, HDS-3 (1961)

Manning's Equation Nomograph

FIGURE

3-7



**Directions for Application:**

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

**Application Form:**

- (a) Selected frequency \_\_\_\_\_ year
- (b)  $P_6 =$  \_\_\_\_\_ in.,  $P_{24} =$  \_\_\_\_\_,  $\frac{P_6}{P_{24}} =$  \_\_\_\_\_ %<sup>(2)</sup>
- (c) Adjusted  $P_6^{(2)} =$  \_\_\_\_\_ in.
- (d)  $t_x =$  \_\_\_\_\_ min.
- (e)  $I =$  \_\_\_\_\_ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

P6	1	1.5	2	2.5	3	3.5	4	4.5	5	5.5	6
5	2.63	3.95	5.27	6.59	7.90	9.22	10.54	11.86	13.17	14.49	15.81
7	2.12	3.18	4.24	5.30	6.36	7.42	8.48	9.54	10.60	11.66	12.72
10	1.68	2.53	3.37	4.21	5.05	5.90	6.74	7.58	8.42	9.27	10.11
15	1.30	1.95	2.59	3.24	3.89	4.54	5.19	5.84	6.49	7.13	7.78
20	1.08	1.62	2.15	2.69	3.23	3.77	4.31	4.85	5.39	5.93	6.46
25	0.93	1.40	1.87	2.33	2.80	3.27	3.73	4.20	4.67	5.13	5.60
30	0.83	1.24	1.66	2.07	2.49	2.90	3.32	3.73	4.15	4.56	4.98
40	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	3.79	4.13
50	0.60	0.90	1.19	1.49	1.79	2.09	2.39	2.69	2.98	3.28	3.58
60	0.53	0.80	1.06	1.33	1.59	1.86	2.12	2.39	2.65	2.92	3.18
90	0.41	0.61	0.82	1.02	1.23	1.43	1.63	1.84	2.04	2.25	2.45
120	0.34	0.51	0.68	0.85	1.02	1.19	1.36	1.53	1.70	1.87	2.04
150	0.29	0.44	0.59	0.73	0.88	1.03	1.18	1.32	1.47	1.62	1.76
180	0.26	0.39	0.52	0.65	0.78	0.91	1.04	1.18	1.31	1.44	1.57
240	0.22	0.33	0.43	0.54	0.65	0.76	0.87	0.98	1.08	1.19	1.30
300	0.19	0.28	0.38	0.47	0.56	0.66	0.75	0.85	0.94	1.03	1.13
360	0.17	0.25	0.33	0.42	0.50	0.58	0.67	0.75	0.84	0.92	1.00

Intensity-Duration Design Chart - Template

FIGURE

3-1

## **CHAPTER 3**

### **HYDROLOGIC ANALYSIS**

#### **3.1 – 50-Year Existing Condition AES Model Output**



50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.110  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 7.06 SUBAREA RUNOFF(CFS) = 13.17  
TOTAL AREA(ACRES) = 7.2 TOTAL RUNOFF(CFS) = 13.38  
TC(MIN.) = 12.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	435.00	DOWNSTREAM(FEET) =	280.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1203.00	CHANNEL SLOPE =	0.1288
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION			
CHANNEL FLOW THRU SUBAREA(CFS) =	13.38		
FLOW VELOCITY(FEET/SEC) =	8.52 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)		
TRAVEL TIME(MIN.) =	2.35	Tc(MIN.) =	14.84
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	103.00 =	2336.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.782
*USER SPECIFIED(SUBAREA):	
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000
SUBAREA AREA(ACRES) =	29.34 SUBAREA RUNOFF(CFS) = 48.97
TOTAL AREA(ACRES) =	36.5 TOTAL RUNOFF(CFS) = 60.94
TC(MIN.) =	14.84

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 113.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	280.00	DOWNSTREAM(FEET) =	269.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	480.00	CHANNEL SLOPE =	0.0229
CHANNEL FLOW THRU SUBAREA(CFS) =	60.94		
FLOW VELOCITY(FEET/SEC) =	6.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)		
TRAVEL TIME(MIN.) =	1.29	Tc(MIN.) =	16.13
LONGEST FLOWPATH FROM NODE	100.00 TO NODE	113.00 =	2816.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	16.13
RAINFALL INTENSITY(INCH/HR) =	2.64
TOTAL STREAM AREA(ACRES) =	36.51
PEAK FLOW RATE(CFS) AT CONFLUENCE =	60.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):	
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00
UPSTREAM ELEVATION(FEET) =	643.00
DOWNSTREAM ELEVATION(FEET) =	633.00
ELEVATION DIFFERENCE(FEET) =	10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!	
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.	
SUBAREA RUNOFF(CFS) =	0.30
TOTAL AREA(ACRES) =	0.09 TOTAL RUNOFF(CFS) = 0.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	633.00	DOWNSTREAM(FEET) =	390.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1383.00	CHANNEL SLOPE =	0.1757
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION			
CHANNEL FLOW THRU SUBAREA(CFS) =	0.30		
FLOW VELOCITY(FEET/SEC) =	2.35 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)		
TRAVEL TIME(MIN.) =	9.82	Tc(MIN.) =	14.00



```

LONGEST FLOWPATH FROM NODE    110.00 TO NODE    112.00 =    1483.00 FEET.
*****
FLOW PROCESS FROM NODE    111.00 TO NODE    112.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.889
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 17.23 SUBAREA RUNOFF(CFS) = 29.87
TOTAL AREA(ACRES) = 17.3 TOTAL RUNOFF(CFS) = 30.02
TC(MIN.) = 14.00
*****
FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 390.00 DOWNSTREAM(FEET) = 269.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1243.00 CHANNEL SLOPE = 0.0973
CHANNEL FLOW THRU SUBAREA(CFS) = 30.02
FLOW VELOCITY(FEET/SEC) = 10.45 (PER LACPCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.98 Tc(MIN.) = 15.98
LONGEST FLOWPATH FROM NODE    110.00 TO NODE    113.00 =    2726.00 FEET.
*****
FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.652
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 19.29 SUBAREA RUNOFF(CFS) = 30.70
TOTAL AREA(ACRES) = 36.6 TOTAL RUNOFF(CFS) = 58.26
TC(MIN.) = 15.98
*****
FLOW PROCESS FROM NODE    113.00 TO NODE    113.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 15.98
RAINFALL INTENSITY(INCH/HR) = 2.65
TOTAL STREAM AREA(ACRES) = 36.61
PEAK FLOW RATE(CFS) AT CONFLUENCE = 58.26

** CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)
1        60.94    16.13    2.636    36.51
2        58.26    15.98    2.652    36.61

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM    RUNOFF    Tc    INTENSITY
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)
1        118.63    15.98    2.652
2        118.85    16.13    2.636

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 118.85 Tc(MIN.) = 16.13
TOTAL AREA(ACRES) = 73.1
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    113.00 =    2816.00 FEET.
*****
FLOW PROCESS FROM NODE    113.00 TO NODE    123.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 269.00 DOWNSTREAM(FEET) = 236.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 972.00 CHANNEL SLOPE = 0.0340
CHANNEL FLOW THRU SUBAREA(CFS) = 118.85
FLOW VELOCITY(FEET/SEC) = 9.21 (PER LACPCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 17.89
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    123.00 =    3788.00 FEET.
*****
FLOW PROCESS FROM NODE    123.00 TO NODE    123.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 17.89
RAINFALL INTENSITY(INCH/HR) = 2.47
TOTAL STREAM AREA(ACRES) = 73.12
PEAK FLOW RATE(CFS) AT CONFLUENCE = 118.85

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 530.00
DOWNSTREAM ELEVATION(FEET) = 520.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.40
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.40

*****
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 520.00 DOWNSTREAM(FEET) = 325.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1285.00 CHANNEL SLOPE = 0.1518
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.40
FLOW VELOCITY(FEET/SEC) = 2.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 9.82 Tc(MIN.) = 14.00
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 122.00 = 1385.00 FEET.

*****
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.889
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 14.79 SUBAREA RUNOFF(CFS) = 25.64
TOTAL AREA(ACRES) = 14.9 TOTAL RUNOFF(CFS) = 25.85
TC(MIN.) = 14.00

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 325.00 DOWNSTREAM(FEET) = 236.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1065.00 CHANNEL SLOPE = 0.0836
CHANNEL FLOW THRU SUBAREA(CFS) = 25.85
FLOW VELOCITY(FEET/SEC) = 9.29 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.91 Tc(MIN.) = 15.91
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 123.00 = 2450.00 FEET.

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.660
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 25.97 SUBAREA RUNOFF(CFS) = 41.45
TOTAL AREA(ACRES) = 40.9 TOTAL RUNOFF(CFS) = 65.25
TC(MIN.) = 15.91

*****
FLOW PROCESS FROM NODE 123.00 TO NODE 123.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 15.91
RAINFALL INTENSITY(INCH/HR) = 2.66

```

TOTAL STREAM AREA(ACRES) = 40.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 65.25

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	118.85	17.89	2.466	73.12
2	65.25	15.91	2.660	40.88

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	175.43	15.91	2.660
2	179.34	17.89	2.466

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 179.34 Tc(MIN.) = 17.89  
TOTAL AREA(ACRES) = 114.0  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 123.00 = 3788.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	236.00	DOWNSTREAM(FEET) =	200.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1970.00	CHANNEL SLOPE =	0.0183
CHANNEL FLOW THRU SUBAREA(CFS) =	179.34		
FLOW VELOCITY(FEET/SEC) =	7.67	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	4.28	Tc(MIN.) =	22.17
LONGEST FLOWPATH FROM NODE	100.00	TO NODE	124.00 = 5758.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.147		
*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000		
SUBAREA AREA(ACRES) =	19.96	SUBAREA RUNOFF(CFS) =	25.72
TOTAL AREA(ACRES) =	134.0	TOTAL RUNOFF(CFS) =	179.34
TC(MIN.) =	22.17		
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE			

\*\*\*\*\*  
FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	22.17
RAINFALL INTENSITY(INCH/HR) =	2.15
TOTAL STREAM AREA(ACRES) =	133.96
PEAK FLOW RATE(CFS) AT CONFLUENCE =	179.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00		
UPSTREAM ELEVATION(FEET) =	650.00		
DOWNSTREAM ELEVATION(FEET) =	640.00		
ELEVATION DIFFERENCE(FEET) =	10.00		
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178		
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!			
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.612		
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.			
SUBAREA RUNOFF(CFS) =	1.58		
TOTAL AREA(ACRES) =	0.47	TOTAL RUNOFF(CFS) =	1.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	640.00	DOWNSTREAM(FEET) =	450.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1167.00	CHANNEL SLOPE =	0.1628
CHANNEL FLOW THRU SUBAREA(CFS) =	1.58		
FLOW VELOCITY(FEET/SEC) =	2.63	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	

TRAVEL TIME(MIN.) = 7.39 Tc(MIN.) = 11.57  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 1267.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.268  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 18.69 SUBAREA RUNOFF(CFS) = 36.64  
TOTAL AREA(ACRES) = 19.2 TOTAL RUNOFF(CFS) = 37.56  
TC(MIN.) = 11.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 360.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1271.00 CHANNEL SLOPE = 0.0708  
CHANNEL FLOW THRU SUBAREA(CFS) = 37.56  
FLOW VELOCITY(FEET/SEC) = 9.49 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.23 Tc(MIN.) = 13.80  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 133.00 = 2538.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.916  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 25.58 SUBAREA RUNOFF(CFS) = 44.75  
TOTAL AREA(ACRES) = 44.7 TOTAL RUNOFF(CFS) = 78.28  
TC(MIN.) = 13.80

\*\*\*\*\*  
FLOW PROCESS FROM NODE 133.00 TO NODE 124.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 360.00 DOWNSTREAM(FEET) = 200.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1666.00 CHANNEL SLOPE = 0.0960  
CHANNEL FLOW THRU SUBAREA(CFS) = 78.28  
FLOW VELOCITY(FEET/SEC) = 7.41 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.75 Tc(MIN.) = 17.54  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 124.00 = 4204.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 133.00 TO NODE 124.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.498  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 22.68 SUBAREA RUNOFF(CFS) = 33.99  
TOTAL AREA(ACRES) = 67.4 TOTAL RUNOFF(CFS) = 101.03  
TC(MIN.) = 17.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.54  
RAINFALL INTENSITY(INCH/HR) = 2.50  
TOTAL STREAM AREA(ACRES) = 67.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 101.03

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	179.34	22.17	2.147	133.96
2	101.03	17.54	2.498	67.42

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	255.23	17.54	2.498
2	266.21	22.17	2.147

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 266.21 Tc(MIN.) = 22.17  
TOTAL AREA(ACRES) = 201.4  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 124.00 = 5758.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 201.4 TC(MIN.) = 22.17  
PEAK FLOW RATE(CFS) = 266.21

=====

END OF RATIONAL METHOD ANALYSIS

## **CHAPTER 3**

### **HYDROLOGIC ANALYSIS**

#### **3.2 – 100-Year Existing Condition AES Model Output**

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2010 Advanced Engineering Software (aes)  
Ver. 17.0 Release Date: 07/01/2010 License ID 1239

Analysis prepared by:

Hunsaker & Associates San Diego, Inc.  
9707 Waples Street  
San Diego, CA 92121

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* Otay Ranch village 4 South \*  
\* 100-year return interval \*  
\* DLN 0924, W.O. 3206-0002 \*  
\*\*\*\*\*

FILE NAME: R:\0924\HYD\CALCS\AES\EX100.DAT  
TIME/DATE OF STUDY: 16:06 02/26/2015

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 2.350  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150
2	17.0	10.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150
3	20.0	12.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150
4	16.0	10.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150
5	26.0	18.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150
6	44.0	12.0	0.020/0.020/0.020	0.50	1.50 0.0313 0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.50 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*\*\*\*\*  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 613.00  
DOWNSTREAM ELEVATION(FEET) = 607.00  
ELEVATION DIFFERENCE(FEET) = 6.00  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.953  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.41  
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.41  
-----

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

\*\*\*\*\*  
ELEVATION DATA: UPSTREAM(FEET) = 607.00 DOWNSTREAM(FEET) = 435.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1033.00 CHANNEL SLOPE = 0.1665  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.41  
FLOW VELOCITY(FEET/SEC) = 2.29 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 7.53 Tc(MIN.) = 12.49  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 1133.00 FEET.  
-----

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

\*\*\*\*\*

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.431  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 7.06 SUBAREA RUNOFF(CFS) = 14.53  
TOTAL AREA(ACRES) = 7.2 TOTAL RUNOFF(CFS) = 14.76  
TC(MIN.) = 12.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	435.00	DOWNSTREAM(FEET) =	280.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1203.00	CHANNEL SLOPE =	0.1288
NOTE: CHANNEL SLOPE OF .1 WAS ASSUMED IN VELOCITY ESTIMATION			
CHANNEL FLOW THRU SUBAREA(CFS) =	14.76		
FLOW VELOCITY(FEET/SEC) =	8.74	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	2.29	Tc(MIN.) =	14.78
LONGEST FLOWPATH FROM NODE	100.00	TO NODE	103.00 = 2336.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.077		
*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000		
SUBAREA AREA(ACRES) =	29.34	SUBAREA RUNOFF(CFS) =	54.17
TOTAL AREA(ACRES) =	36.5	TOTAL RUNOFF(CFS) =	67.41
TC(MIN.) =	14.78		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 113.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	280.00	DOWNSTREAM(FEET) =	269.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	480.00	CHANNEL SLOPE =	0.0229
CHANNEL FLOW THRU SUBAREA(CFS) =	67.41		
FLOW VELOCITY(FEET/SEC) =	6.39	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	1.25	Tc(MIN.) =	16.03
LONGEST FLOWPATH FROM NODE	100.00	TO NODE	113.00 = 2816.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 113.00 TO NODE 113.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	16.03
RAINFALL INTENSITY(INCH/HR) =	2.92
TOTAL STREAM AREA(ACRES) =	36.51
PEAK FLOW RATE(CFS) AT CONFLUENCE =	67.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00		
UPSTREAM ELEVATION(FEET) =	643.00		
DOWNSTREAM ELEVATION(FEET) =	633.00		
ELEVATION DIFFERENCE(FEET) =	10.00		
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178		
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!			
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.192		
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.			
SUBAREA RUNOFF(CFS) =	0.33		
TOTAL AREA(ACRES) =	0.09	TOTAL RUNOFF(CFS) =	0.33

\*\*\*\*\*  
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	633.00	DOWNSTREAM(FEET) =	390.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1383.00	CHANNEL SLOPE =	0.1757
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION			
CHANNEL FLOW THRU SUBAREA(CFS) =	0.33		
FLOW VELOCITY(FEET/SEC) =	2.35	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	9.82	Tc(MIN.) =	14.00



```

LONGEST FLOWPATH FROM NODE    110.00 TO NODE    112.00 =    1483.00 FEET.
*****
FLOW PROCESS FROM NODE    111.00 TO NODE    112.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.187
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 17.23 SUBAREA RUNOFF(CFS) = 32.95
TOTAL AREA(ACRES) = 17.3 TOTAL RUNOFF(CFS) = 33.12
TC(MIN.) = 14.00
*****
FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 390.00 DOWNSTREAM(FEET) = 269.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1243.00 CHANNEL SLOPE = 0.0973
CHANNEL FLOW THRU SUBAREA(CFS) = 33.12
FLOW VELOCITY(FEET/SEC) = 10.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.93 Tc(MIN.) = 15.93
LONGEST FLOWPATH FROM NODE    110.00 TO NODE    113.00 =    2726.00 FEET.
*****
FLOW PROCESS FROM NODE    112.00 TO NODE    113.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.933
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 19.29 SUBAREA RUNOFF(CFS) = 33.94
TOTAL AREA(ACRES) = 36.6 TOTAL RUNOFF(CFS) = 64.42
TC(MIN.) = 15.93
*****
FLOW PROCESS FROM NODE    113.00 TO NODE    113.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 15.93
RAINFALL INTENSITY(INCH/HR) = 2.93
TOTAL STREAM AREA(ACRES) = 36.61
PEAK FLOW RATE(CFS) AT CONFLUENCE = 64.42

** CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)
1        67.41    16.03    2.920    36.51
2        64.42    15.93    2.933    36.61

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM    RUNOFF    Tc    INTENSITY
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)
1        131.38    15.93    2.933
2        131.55    16.03    2.920

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 131.55 Tc(MIN.) = 16.03
TOTAL AREA(ACRES) = 73.1
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    113.00 =    2816.00 FEET.
*****
FLOW PROCESS FROM NODE    113.00 TO NODE    123.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 269.00 DOWNSTREAM(FEET) = 236.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 972.00 CHANNEL SLOPE = 0.0340
CHANNEL FLOW THRU SUBAREA(CFS) = 131.55
FLOW VELOCITY(FEET/SEC) = 9.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.70 Tc(MIN.) = 17.74
LONGEST FLOWPATH FROM NODE    100.00 TO NODE    123.00 =    3788.00 FEET.
*****
FLOW PROCESS FROM NODE    123.00 TO NODE    123.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 17.74
RAINFALL INTENSITY(INCH/HR) = 2.74
TOTAL STREAM AREA(ACRES) = 73.12
PEAK FLOW RATE(CFS) AT CONFLUENCE = 131.55

*****
FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 530.00
DOWNSTREAM ELEVATION(FEET) = 520.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.12 TOTAL RUNOFF(CFS) = 0.45

*****
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 520.00 DOWNSTREAM(FEET) = 325.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1285.00 CHANNEL SLOPE = 0.1518
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.45
FLOW VELOCITY(FEET/SEC) = 2.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 9.82 Tc(MIN.) = 14.00
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 122.00 = 1385.00 FEET.

*****
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.188
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 14.79 SUBAREA RUNOFF(CFS) = 28.29
TOTAL AREA(ACRES) = 14.9 TOTAL RUNOFF(CFS) = 28.52
TC(MIN.) = 14.00

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 325.00 DOWNSTREAM(FEET) = 236.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1065.00 CHANNEL SLOPE = 0.0836
CHANNEL FLOW THRU SUBAREA(CFS) = 28.52
FLOW VELOCITY(FEET/SEC) = 9.55 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 1.86 Tc(MIN.) = 15.85
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 123.00 = 2450.00 FEET.

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 123.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.941
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 25.97 SUBAREA RUNOFF(CFS) = 45.83
TOTAL AREA(ACRES) = 40.9 TOTAL RUNOFF(CFS) = 72.14
TC(MIN.) = 15.85

*****
FLOW PROCESS FROM NODE 123.00 TO NODE 123.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 15.85
RAINFALL INTENSITY(INCH/HR) = 2.94

```

TOTAL STREAM AREA(ACRES) = 40.88  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 72.14

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	131.55	17.74	2.736	73.12
2	72.14	15.85	2.941	40.88

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	194.51	15.85	2.941
2	198.66	17.74	2.736

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 198.66 Tc(MIN.) = 17.74  
TOTAL AREA(ACRES) = 114.0  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 123.00 = 3788.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	236.00	DOWNSTREAM(FEET) =	200.00	
CHANNEL LENGTH THRU SUBAREA(FEET) =	1970.00	CHANNEL SLOPE =	0.0183	
CHANNEL FLOW THRU SUBAREA(CFS) =	198.66			
FLOW VELOCITY(FEET/SEC) =	7.91	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)		
TRAVEL TIME(MIN.) =	4.15	Tc(MIN.) =	21.89	
LONGEST FLOWPATH FROM NODE	100.00	TO NODE	124.00 =	5758.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 123.00 TO NODE 124.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.389		
*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000		
SUBAREA AREA(ACRES) =	19.96	SUBAREA RUNOFF(CFS) =	28.61
TOTAL AREA(ACRES) =	134.0	TOTAL RUNOFF(CFS) =	198.66
TC(MIN.) =	21.89		
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE			

\*\*\*\*\*  
FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	21.89
RAINFALL INTENSITY(INCH/HR) =	2.39
TOTAL STREAM AREA(ACRES) =	133.96
PEAK FLOW RATE(CFS) AT CONFLUENCE =	198.66

\*\*\*\*\*  
FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00		
UPSTREAM ELEVATION(FEET) =	650.00		
DOWNSTREAM ELEVATION(FEET) =	640.00		
ELEVATION DIFFERENCE(FEET) =	10.00		
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178		
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!			
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.192		
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.			
SUBAREA RUNOFF(CFS) =	1.75		
TOTAL AREA(ACRES) =	0.47	TOTAL RUNOFF(CFS) =	1.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	640.00	DOWNSTREAM(FEET) =	450.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	1167.00	CHANNEL SLOPE =	0.1628
CHANNEL FLOW THRU SUBAREA(CFS) =	1.75		
FLOW VELOCITY(FEET/SEC) =	2.72	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	

TRAVEL TIME(MIN.) = 7.15 Tc(MIN.) = 11.33  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 1267.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.654  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 18.69 SUBAREA RUNOFF(CFS) = 40.97  
TOTAL AREA(ACRES) = 19.2 TOTAL RUNOFF(CFS) = 42.00  
TC(MIN.) = 11.33

\*\*\*\*\*  
FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 360.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1271.00 CHANNEL SLOPE = 0.0708  
CHANNEL FLOW THRU SUBAREA(CFS) = 42.00  
FLOW VELOCITY(FEET/SEC) = 9.80 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 2.16 Tc(MIN.) = 13.49  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 133.00 = 2538.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.264  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 25.58 SUBAREA RUNOFF(CFS) = 50.10  
TOTAL AREA(ACRES) = 44.7 TOTAL RUNOFF(CFS) = 87.63  
TC(MIN.) = 13.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 133.00 TO NODE 124.00 IS CODE = 53

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 360.00 DOWNSTREAM(FEET) = 200.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 1666.00 CHANNEL SLOPE = 0.0960  
CHANNEL FLOW THRU SUBAREA(CFS) = 87.63  
FLOW VELOCITY(FEET/SEC) = 7.70 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 3.61 Tc(MIN.) = 17.10  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 124.00 = 4204.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 133.00 TO NODE 124.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.802  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 22.68 SUBAREA RUNOFF(CFS) = 38.12  
TOTAL AREA(ACRES) = 67.4 TOTAL RUNOFF(CFS) = 113.33  
TC(MIN.) = 17.10

\*\*\*\*\*  
FLOW PROCESS FROM NODE 124.00 TO NODE 124.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 17.10  
RAINFALL INTENSITY(INCH/HR) = 2.80  
TOTAL STREAM AREA(ACRES) = 67.42  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 113.33

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	198.66	21.89	2.389	133.96
2	113.33	17.10	2.802	67.42

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	282.73	17.10	2.802
2	295.29	21.89	2.389

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 295.29 Tc(MIN.) = 21.89

TOTAL AREA(ACRES) = 201.4

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 124.00 = 5758.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 201.4 TC(MIN.) = 21.89

PEAK FLOW RATE(CFS) = 295.29

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **CHAPTER 3**

### **HYDROLOGIC ANALYSIS**

#### **3.3 – 50-Year Developed Condition AES Model Output**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2015 Advanced Engineering Software (aes)
Ver. 22.0 Release Date: 07/01/2015 License ID 1239

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*
\* Otay Ranch Village 4 South \*
\* 50-year return interval \*
\* DLN:0924, W.O. 3206-0002 \*
\*\*\*\*\*

FILE NAME: R:\0924\HYD\CALCS\AES\PR50.DAT
TIME/DATE OF STUDY: 11:34 06/22/2016

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 50.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.130
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*
Table with 10 columns: NO., HALF-WIDTH (FT), CROWN CROSSFALL (FT), STREET-CROSSFALL IN-/OUT-/SIDE, PARK-/WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), GEOMETRIES LIP (FT), HIKE (FT), MANNING FACTOR (n). Rows 1-6.

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.50 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .8500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00
UPSTREAM ELEVATION(FEET) = 437.63
DOWNSTREAM ELEVATION(FEET) = 437.02
ELEVATION DIFFERENCE(FEET) = 0.61
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.467
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.96
TOTAL AREA(ACRES) = 0.41 TOTAL RUNOFF(CFS) = 1.96

\*\*\*\*\*
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 62
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 6 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 437.02 DOWNSTREAM ELEVATION(FEET) = 432.91
STREET LENGTH(FEET) = 413.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 12.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.00
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 9.99
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.24
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.73
STREET FLOW TRAVEL TIME(MIN.) = 3.07 Tc(MIN.) = 6.54
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.722
\*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .8500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
SUBAREA AREA(ACRES) = 1.51 SUBAREA RUNOFF(CFS) = 6.06
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 7.71

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.01
FLOW VELOCITY(FEET/SEC.) = 2.47 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.90
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 473.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 428.00 DOWNSTREAM(FEET) = 427.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.16
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.71
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 6.64
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 523.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====

\*\*\*\*\*
FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
\*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 525.00
DOWNSTREAM ELEVATION(FEET) = 515.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 31
=====



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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 515.00 DOWNSTREAM(FEET) = 451.00
FLOW LENGTH(FEET) = 548.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.36
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.37
PIPE TRAVEL TIME(MIN.) = 1.44 Tc(MIN.) = 5.61
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 648.00 FEET.

*****
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.208
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 2.16 SUBAREA RUNOFF(CFS) = 6.75
TOTAL AREA(ACRES) = 2.3 TOTAL RUNOFF(CFS) = 7.09
TC(MIN.) = 5.61

*****
FLOW PROCESS FROM NODE 112.00 TO NODE 117.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 446.00 DOWNSTREAM(FEET) = 435.00
FLOW LENGTH(FEET) = 254.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.63
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.09
PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 6.01
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 117.00 = 902.00 FEET.

*****
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.01
RAINFALL INTENSITY(INCH/HR) = 4.98
TOTAL STREAM AREA(ACRES) = 2.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.09

*****
FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 526.45
DOWNSTREAM ELEVATION(FEET) = 525.80
ELEVATION DIFFERENCE(FEET) = 0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555
SUBAREA RUNOFF(CFS) = 1.12
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 1.12

*****
FLOW PROCESS FROM NODE 116.00 TO NODE 117.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STANDARD CURB SECTION USED)<<<<<
=====

```

UPSTREAM ELEVATION(FEET) = 525.80 DOWNSTREAM ELEVATION(FEET) = 438.25  
STREET LENGTH(FEET) = 721.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.49  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.21  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.65  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.80  
STREET FLOW TRAVEL TIME(MIN.) = 1.81 Tc(MIN.) = 6.89  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.565  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 4.28 SUBAREA RUNOFF(CFS) = 14.65  
TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 15.58

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.53  
FLOW VELOCITY(FEET/SEC.) = 7.59 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.40  
LONGEST FLOWPATH FROM NODE 115.00 TO NODE 117.00 = 786.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.89  
RAINFALL INTENSITY(INCH/HR) = 4.57  
TOTAL STREAM AREA(ACRES) = 4.55  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.58

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.09	6.01	4.983	2.27
2	15.58	6.89	4.565	4.55

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	20.70	6.01	4.983
2	22.08	6.89	4.565

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 22.08 Tc(MIN.) = 6.89  
TOTAL AREA(ACRES) = 6.8  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 117.00 = 902.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 117.00 TO NODE 118.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 433.00 DOWNSTREAM(FEET) = 427.00  
FLOW LENGTH(FEET) = 272.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 17.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.58  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 22.08  
PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 7.31  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 118.00 = 1174.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
-----  
TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.31  
RAINFALL INTENSITY(INCH/HR) = 4.39  
TOTAL STREAM AREA(ACRES) = 6.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.08

\*\*\*\*\*  
FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
-----  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 451.55  
DOWNSTREAM ELEVATION(FEET) = 450.90  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
SUBAREA RUNOFF(CFS) = 1.29  
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 1.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
-----  
UPSTREAM ELEVATION(FEET) = 446.20 DOWNSTREAM ELEVATION(FEET) = 430.50  
STREET LENGTH(FEET) = 446.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00  
  
DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.12  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.81  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.11  
STREET FLOW TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 7.03  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.504  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.84 SUBAREA RUNOFF(CFS) = 9.59  
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 10.64

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.53  
FLOW VELOCITY(FEET/SEC.) = 4.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.46  
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 122.00 = 511.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 81

```

-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.504
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (HILLY) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7402
SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.59
TOTAL AREA(ACRES) = 3.4 TOTAL RUNOFF(CFS) = 11.24
TC(MIN.) = 7.03

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 118.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.03
RAINFALL INTENSITY(INCH/HR) = 4.50
TOTAL STREAM AREA(ACRES) = 3.37
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.24

*****
FLOW PROCESS FROM NODE 125.00 TO NODE 126.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 453.85
DOWNSTREAM ELEVATION(FEET) = 453.20
ELEVATION DIFFERENCE(FEET) = 0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
         (Reference: Table 3-1B of Hydrology Manual)
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555
SUBAREA RUNOFF(CFS) = 0.37
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.37

*****
FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 453.20 DOWNSTREAM ELEVATION(FEET) = 430.50
STREET LENGTH(FEET) = 655.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.18
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 7.67
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.66
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.02
STREET FLOW TRAVEL TIME(MIN.) = 2.98 Tc(MIN.) = 8.06
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.125
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750
SUBAREA AREA(ACRES) = 3.06 SUBAREA RUNOFF(CFS) = 9.47
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 9.74

```

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.16  
 FLOW VELOCITY(FEET/SEC.) = 4.24 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.40  
 LONGEST FLOWPATH FROM NODE 125.00 TO NODE 127.00 = 720.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 127.00 TO NODE 118.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.06  
 RAINFALL INTENSITY(INCH/HR) = 4.12  
 TOTAL STREAM AREA(ACRES) = 3.15  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.74

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	22.08	7.31	4.391	6.82
2	11.24	7.03	4.504	3.37
3	9.74	8.06	4.125	3.15

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	41.26	7.03	4.504
2	41.88	7.31	4.391
3	40.77	8.06	4.125

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 41.88 Tc(MIN.) = 7.31  
 TOTAL AREA(ACRES) = 13.3  
 LONGEST FLOWPATH FROM NODE 110.00 TO NODE 118.00 = 1174.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 118.00 TO NODE 103.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 427.00 DOWNSTREAM(FEET) = 426.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.43  
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 41.88  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 7.57  
 LONGEST FLOWPATH FROM NODE 110.00 TO NODE 103.00 = 1304.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 130.00 TO NODE 130.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	41.88	7.57	4.294	13.34

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 130.00 = 1304.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.71	6.64	4.674	1.92

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 130.00 = 523.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
---------------	--------------	-----------	-----------------------

1 44.42 6.64 4.674  
2 48.95 7.57 4.294

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 48.95 Tc(MIN.) = 7.57  
TOTAL AREA(ACRES) = 15.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 12  
-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 128.00 IS CODE = 31  
-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 426.00 DOWNSTREAM(FEET) = 422.00  
FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.33  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 48.95  
PIPE TRAVEL TIME(MIN.) = 0.82 Tc(MIN.) = 8.39  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 128.00 = 1764.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 128.00 TO NODE 128.00 IS CODE = 1  
-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.39  
RAINFALL INTENSITY(INCH/HR) = 4.02  
TOTAL STREAM AREA(ACRES) = 15.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 48.95

\*\*\*\*\*  
FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 444.15  
DOWNSTREAM ELEVATION(FEET) = 443.50  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 31  
-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 435.80 DOWNSTREAM(FEET) = 428.00  
FLOW LENGTH(FEET) = 995.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.58  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.42  
PIPE TRAVEL TIME(MIN.) = 6.43 Tc(MIN.) = 11.51  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 1060.00 FEET.

```

*****
FLOW PROCESS FROM NODE      131.00 TO NODE      132.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
    50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.278
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7500
SUBAREA AREA(ACRES) =      6.96  SUBAREA RUNOFF(CFS) =   17.11
TOTAL AREA(ACRES) =      7.1  TOTAL RUNOFF(CFS) =   17.36
TC(MIN.) =   11.51

*****
FLOW PROCESS FROM NODE      132.00 TO NODE      128.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  438.50  DOWNSTREAM(FEET) =  422.00
FLOW LENGTH(FEET) =  115.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  8.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  20.91
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =   17.36
PIPE TRAVEL TIME(MIN.) =  0.09  Tc(MIN.) =  11.60
LONGEST FLOWPATH FROM NODE      130.00 TO NODE      128.00 =   1175.00 FEET.

*****
FLOW PROCESS FROM NODE      128.00 TO NODE      128.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =  11.60
RAINFALL INTENSITY(INCH/HR) =  3.26
TOTAL STREAM AREA(ACRES) =  7.06
PEAK FLOW RATE(CFS) AT CONFLUENCE =   17.36

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
    1         48.95      8.39      4.018      15.26
    2         17.36     11.60      3.261      7.06

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR  2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
    1         61.51      8.39      4.018
    2         57.08     11.60      3.261

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =   61.51  Tc(MIN.) =   8.39
TOTAL AREA(ACRES) =   22.3
LONGEST FLOWPATH FROM NODE      110.00 TO NODE      128.00 =   1764.00 FEET.

*****
FLOW PROCESS FROM NODE      128.00 TO NODE      137.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  422.00  DOWNSTREAM(FEET) =  414.00
FLOW LENGTH(FEET) =  610.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  11.50
ESTIMATED PIPE DIAMETER(INCH) =  36.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =   61.51
PIPE TRAVEL TIME(MIN.) =  0.88  Tc(MIN.) =   9.28
LONGEST FLOWPATH FROM NODE      110.00 TO NODE      137.00 =   2374.00 FEET.

```

\*\*\*\*\*  
FLOW PROCESS FROM NODE 137.00 TO NODE 137.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.28
RAINFALL INTENSITY(INCH/HR) =	3.77
TOTAL STREAM AREA(ACRES) =	22.32
PEAK FLOW RATE(CFS) AT CONFLUENCE =	61.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 135.00 TO NODE 136.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

PAVED SURFACE RUNOFF COEFFICIENT =	.8500
INITIAL SUBAREA FLOW-LENGTH(FEET) =	103.00
UPSTREAM ELEVATION(FEET) =	432.50
DOWNSTREAM ELEVATION(FEET) =	431.60
ELEVATION DIFFERENCE(FEET) =	0.90
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	3.568

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 57.48  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc =	5-MINUTE.
SUBAREA RUNOFF(CFS) =	1.19
TOTAL AREA(ACRES) =	0.25
TOTAL RUNOFF(CFS) =	1.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	430.75	DOWNSTREAM ELEVATION(FEET) =	418.50
STREET LENGTH(FEET) =	1000.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	44.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	22.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	2
STREET PARKWAY CROSSFALL(DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	8.12
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:	
STREET FLOW DEPTH(FEET) =	0.36
HALFSTREET FLOOD WIDTH(FEET) =	11.71
AVERAGE FLOW VELOCITY(FEET/SEC.) =	2.72
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =	0.98
STREET FLOW TRAVEL TIME(MIN.) =	6.12
Tc(MIN.) =	9.69
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.663

\*USER SPECIFIED(SUBAREA):

COMMERCIAL AREA RUNOFF COEFFICIENT =	.8500
AREA-AVERAGE RUNOFF COEFFICIENT =	0.850
SUBAREA AREA(ACRES) =	4.30
SUBAREA RUNOFF(CFS) =	13.39
TOTAL AREA(ACRES) =	4.6
PEAK FLOW RATE(CFS) =	14.17

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) =	0.42	HALFSTREET FLOOD WIDTH(FEET) =	14.75
FLOW VELOCITY(FEET/SEC.) =	3.09	DEPTH*VELOCITY(FT*FT/SEC.) =	1.30
LONGEST FLOWPATH FROM NODE 135.00 TO NODE 137.00 =	1103.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 137.00 TO NODE 137.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<



```

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.69
RAINFALL INTENSITY(INCH/HR) = 3.66
TOTAL STREAM AREA(ACRES) = 4.55
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.17

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
1           61.51      9.28    3.767          22.32
2           14.17      9.69    3.663          4.55

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
1           75.08      9.28    3.767
2           73.99      9.69    3.663

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 75.08   Tc(MIN.) = 9.28
TOTAL AREA(ACRES) = 26.9
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 137.00 = 2374.00 FEET.

*****
FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 412.00 DOWNSTREAM(FEET) = 411.00
FLOW LENGTH(FEET) = 75.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 27.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.19
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 75.08
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 9.38
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 138.00 = 2449.00 FEET.

*****
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====
*****
FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 460.00
DOWNSTREAM ELEVATION(FEET) = 450.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.67
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.67

*****
FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 425.00
FLOW LENGTH(FEET) = 652.00 MANNING'S N = 0.013

```

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.14
ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.67
PIPE TRAVEL TIME(MIN.) = 2.11    Tc(MIN.) = 6.29
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 142.00 = 752.00 FEET.

*****
FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.839
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 2.56    SUBAREA RUNOFF(CFS) = 7.43
TOTAL AREA(ACRES) = 2.8    TOTAL RUNOFF(CFS) = 8.01
TC(MIN.) = 6.29

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 147.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 420.00    DOWNSTREAM(FEET) = 417.00
FLOW LENGTH(FEET) = 271.00    MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.54
ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.01
PIPE TRAVEL TIME(MIN.) = 0.69    Tc(MIN.) = 6.98
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 147.00 = 1023.00 FEET.

*****
FLOW PROCESS FROM NODE 147.00 TO NODE 147.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.98
RAINFALL INTENSITY(INCH/HR) = 4.52
TOTAL STREAM AREA(ACRES) = 2.76
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.01

*****
FLOW PROCESS FROM NODE 145.00 TO NODE 146.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 449.15
DOWNSTREAM ELEVATION(FEET) = 448.50
ELEVATION DIFFERENCE(FEET) = 0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555
SUBAREA RUNOFF(CFS) = 0.46
TOTAL AREA(ACRES) = 0.11    TOTAL RUNOFF(CFS) = 0.46

*****
FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 448.50    DOWNSTREAM ELEVATION(FEET) = 421.50
STREET LENGTH(FEET) = 614.00    CURB HEIGHT(INCHES) = 6.0

```

STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.29  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 7.31  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.05  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.10  
STREET FLOW TRAVEL TIME(MIN.) = 2.53 Tc(MIN.) = 7.60  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.282  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.98 SUBAREA RUNOFF(CFS) = 9.57  
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 9.92

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.72  
FLOW VELOCITY(FEET/SEC.) = 4.67 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.50  
LONGEST FLOWPATH FROM NODE 145.00 TO NODE 147.00 = 679.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 147.00 TO NODE 147.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.60  
RAINFALL INTENSITY(INCH/HR) = 4.28  
TOTAL STREAM AREA(ACRES) = 3.09  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.92

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.01	6.98	4.525	2.76
2	9.92	7.60	4.282	3.09

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	17.12	6.98	4.525
2	17.51	7.60	4.282

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 17.51 Tc(MIN.) = 7.60  
TOTAL AREA(ACRES) = 5.8  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 147.00 = 1023.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 147.00 TO NODE 148.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 417.00 DOWNSTREAM(FEET) = 411.00  
FLOW LENGTH(FEET) = 192.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.36  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 17.51  
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 7.89

```

LONGEST FLOWPATH FROM NODE    140.00 TO NODE    148.00 =    1215.00 FEET.
*****
FLOW PROCESS FROM NODE    148.00 TO NODE    148.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    7.89
RAINFALL INTENSITY(INCH/HR) =    4.18
TOTAL STREAM AREA(ACRES) =    5.85
PEAK FLOW RATE(CFS) AT CONFLUENCE =    17.51
*****
FLOW PROCESS FROM NODE    150.00 TO NODE    151.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    453.45
DOWNSTREAM ELEVATION(FEET) =    452.80
ELEVATION DIFFERENCE(FEET) =    0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =    5.079
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =    5.555
SUBAREA RUNOFF(CFS) =    0.42
TOTAL AREA(ACRES) =    0.10  TOTAL RUNOFF(CFS) =    0.42
*****
FLOW PROCESS FROM NODE    151.00 TO NODE    152.00 IS CODE =    61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =    452.80  DOWNSTREAM ELEVATION(FEET) =    415.80
STREET LENGTH(FEET) =    900.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    8.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =    0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    5.44
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.28
HALFSTREET FLOOD WIDTH(FEET) =    7.57
AVERAGE FLOW VELOCITY(FEET/SEC.) =    3.94
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.09
STREET FLOW TRAVEL TIME(MIN.) =    3.81  Tc(MIN.) =    8.89
  50 YEAR RAINFALL INTENSITY(INCH/HOUR) =    3.873
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT =    0.750
SUBAREA AREA(ACRES) =    3.39  SUBAREA RUNOFF(CFS) =    9.85
TOTAL AREA(ACRES) =    3.5  PEAK FLOW RATE(CFS) =    10.14

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =    0.33  HALFSTREET FLOOD WIDTH(FEET) =    9.97
FLOW VELOCITY(FEET/SEC.) =    4.56  DEPTH*VELOCITY(FT*FT/SEC.) =    1.48
LONGEST FLOWPATH FROM NODE    150.00 TO NODE    152.00 =    965.00 FEET.
*****
FLOW PROCESS FROM NODE    152.00 TO NODE    148.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =    8.89

```

RAINFALL INTENSITY(INCH/HR) = 3.87  
TOTAL STREAM AREA(ACRES) = 3.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.14

\*\*\*\*\*  
FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 430.25  
DOWNSTREAM ELEVATION(FEET) = 429.60  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
SUBAREA RUNOFF(CFS) = 0.42  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 156.00 TO NODE 157.00 IS CODE = 61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 429.60 DOWNSTREAM ELEVATION(FEET) = 415.80  
STREET LENGTH(FEET) = 476.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.33  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.23  
HALFSTREET FLOOD WIDTH(FEET) = 5.28  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.93  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.68  
STREET FLOW TRAVEL TIME(MIN.) = 2.71 Tc(MIN.) = 7.79  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.217

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 3.80  
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 4.11

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 7.16  
FLOW VELOCITY(FEET/SEC.) = 3.26 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.88  
LONGEST FLOWPATH FROM NODE 155.00 TO NODE 157.00 = 541.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 157.00 TO NODE 148.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.79  
RAINFALL INTENSITY(INCH/HR) = 4.22  
TOTAL STREAM AREA(ACRES) = 1.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.11

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	17.51	7.89	4.183	5.85
2	10.14	8.89	3.873	3.49
3	4.11	7.79	4.217	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	30.36	7.79	4.217
2	30.58	7.89	4.183
3	30.12	8.89	3.873

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.58 Tc(MIN.) = 7.89  
TOTAL AREA(ACRES) = 10.6  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 148.00 = 1215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 148.00 TO NODE 138.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----  
ELEVATION DATA: UPSTREAM(FEET) = 411.00 DOWNSTREAM(FEET) = 410.00  
FLOW LENGTH(FEET) = 122.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.08  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 30.58  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 8.14  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 138.00 = 1337.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
-----

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	30.58	8.14	4.099	10.64

LONGEST FLOWPATH FROM NODE 140.00 TO NODE 138.00 = 1337.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	75.08	9.38	3.740	26.87

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 138.00 = 2449.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	95.73	8.14	4.099
2	102.98	9.38	3.740

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 102.98 Tc(MIN.) = 9.38  
TOTAL AREA(ACRES) = 37.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<  
-----

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 162.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----

ELEVATION DATA: UPSTREAM(FEET) = 411.00 DOWNSTREAM(FEET) = 362.00  
FLOW LENGTH(FEET) = 987.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.36  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 102.98  
PIPE TRAVEL TIME(MIN.) = 0.77 Tc(MIN.) = 10.15  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.15  
RAINFALL INTENSITY(INCH/HR) = 3.55  
TOTAL STREAM AREA(ACRES) = 37.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 102.98

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 161.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
PAVED SURFACE RUNOFF COEFFICIENT = .8500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 419.00  
DOWNSTREAM ELEVATION(FEET) = 415.50  
ELEVATION DIFFERENCE(FEET) = 3.50  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.692  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 82.50  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.10  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 1.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 415.50 DOWNSTREAM ELEVATION(FEET) = 367.00  
STREET LENGTH(FEET) = 928.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 22.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.92  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.79  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.08  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.63  
STREET FLOW TRAVEL TIME(MIN.) = 3.05 Tc(MIN.) = 5.74  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.134  
\*USER SPECIFIED(SUBAREA):  
PAVED SURFACE RUNOFF COEFFICIENT = .7200  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.725  
SUBAREA AREA(ACRES) = 5.23 SUBAREA RUNOFF(CFS) = 19.33  
TOTAL AREA(ACRES) = 5.5 PEAK FLOW RATE(CFS) = 20.34

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.67  
FLOW VELOCITY(FEET/SEC.) = 5.90 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.24  
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 162.00 = 1028.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.74  
RAINFALL INTENSITY(INCH/HR) = 5.13  
TOTAL STREAM AREA(ACRES) = 5.46  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.34

\*\* CONFLUENCE DATA \*\*  
STREAM RUNOFF Tc INTENSITY AREA  
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)  
1 102.98 10.15 3.555 37.51  
2 20.34 5.74 5.134 5.46

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*  
STREAM RUNOFF Tc INTENSITY  
NUMBER (CFS) (MIN.) (INCH/HOUR)  
1 78.58 5.74 5.134  
2 117.07 10.15 3.555

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 117.07 Tc(MIN.) = 10.15  
TOTAL AREA(ACRES) = 43.0  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 170.00 TO NODE 171.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 556.05  
DOWNSTREAM ELEVATION(FEET) = 555.40  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
SUBAREA RUNOFF(CFS) = 0.75  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 171.00 TO NODE 172.00 IS CODE = 61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 555.40 DOWNSTREAM ELEVATION(FEET) = 529.00  
STREET LENGTH(FEET) = 620.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020



SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.99  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 8.41  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.24  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.25  
STREET FLOW TRAVEL TIME(MIN.) = 2.44 Tc(MIN.) = 7.52  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.314  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 3.82 SUBAREA RUNOFF(CFS) = 12.36  
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 12.94

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 10.97  
FLOW VELOCITY(FEET/SEC.) = 4.90 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.69  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 172.00 = 685.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 172.00 TO NODE 177.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 524.00 DOWNSTREAM(FEET) = 479.00  
FLOW LENGTH(FEET) = 483.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.52  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 12.94  
PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 8.00  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 177.00 = 1168.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.00  
RAINFALL INTENSITY(INCH/HR) = 4.14  
TOTAL STREAM AREA(ACRES) = 4.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.94

\*\*\*\*\*  
FLOW PROCESS FROM NODE 175.00 TO NODE 176.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 529.95  
DOWNSTREAM ELEVATION(FEET) = 529.30  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
SUBAREA RUNOFF(CFS) = 0.67  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 529.30 DOWNSTREAM ELEVATION(FEET) = 484.00

STREET LENGTH(FEET) = 424.70 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.22  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.79  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.76  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.39  
STREET FLOW TRAVEL TIME(MIN.) = 1.23 Tc(MIN.) = 6.31  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.831  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.51 SUBAREA RUNOFF(CFS) = 9.09  
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 9.67

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.92  
FLOW VELOCITY(FEET/SEC.) = 6.48 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.85  
LONGEST FLOWPATH FROM NODE 175.00 TO NODE 177.00 = 489.70 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.31  
RAINFALL INTENSITY(INCH/HR) = 4.83  
TOTAL STREAM AREA(ACRES) = 2.67  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 180.00 TO NODE 181.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 643.00  
DOWNSTREAM ELEVATION(FEET) = 633.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.24  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 181.00 TO NODE 182.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 633.00 DOWNSTREAM(FEET) = 500.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 857.00 CHANNEL SLOPE = 0.1552  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.24  
FLOW VELOCITY(FEET/SEC) = 2.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.47 Tc(MIN.) = 10.65  
LONGEST FLOWPATH FROM NODE 180.00 TO NODE 182.00 = 957.00 FEET.

\*\*\*\*\*

```

FLOW PROCESS FROM NODE      181.00 TO NODE      182.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.446
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) =      3.50  SUBAREA RUNOFF(CFS) =      7.24
TOTAL AREA(ACRES) =      3.6    TOTAL RUNOFF(CFS) =      7.38
TC(MIN.) =  10.65

```

```

*****
FLOW PROCESS FROM NODE      183.00 TO NODE      182.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.446
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) =      1.00  SUBAREA RUNOFF(CFS) =      2.07
TOTAL AREA(ACRES) =      4.6    TOTAL RUNOFF(CFS) =      9.45
TC(MIN.) =  10.65

```

```

*****
FLOW PROCESS FROM NODE      182.00 TO NODE      177.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  495.00  DOWNSTREAM(FEET) =  479.00
FLOW LENGTH(FEET) =  160.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  6.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  15.58
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =      9.45
PIPE TRAVEL TIME(MIN.) =  0.17    Tc(MIN.) =  10.82
LONGEST FLOWPATH FROM NODE      180.00 TO NODE      177.00 =  1117.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE      177.00 TO NODE      177.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =  3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  3 ARE:
TIME OF CONCENTRATION(MIN.) =  10.82
RAINFALL INTENSITY(INCH/HR) =  3.41
TOTAL STREAM AREA(ACRES) =  4.57
PEAK FLOW RATE(CFS) AT CONFLUENCE =      9.45

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	12.94	8.00	4.143	4.00
2	9.67	6.31	4.831	2.67
3	9.45	10.82	3.410	4.57

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	25.38	6.31	4.831
2	28.23	8.00	4.143
3	26.93	10.82	3.410

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 28.23 Tc(MIN.) = 8.00  
TOTAL AREA(ACRES) = 11.2  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 177.00 = 1168.00 FEET.

```

*****
FLOW PROCESS FROM NODE      177.00 TO NODE      187.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   479.00  DOWNSTREAM(FEET) =   425.00
FLOW LENGTH(FEET) =   570.00  MANNING'S N =   0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   19.69
ESTIMATED PIPE DIAMETER(INCH) =   18.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =          28.23
PIPE TRAVEL TIME(MIN.) =   0.48  Tc(MIN.) =    8.49
LONGEST FLOWPATH FROM NODE      170.00 TO NODE      187.00 =   1738.00 FEET.
*****
FLOW PROCESS FROM NODE      187.00 TO NODE      187.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.49
RAINFALL INTENSITY(INCH/HR) =    3.99
TOTAL STREAM AREA(ACRES) =    11.24
PEAK FLOW RATE(CFS) AT CONFLUENCE =    28.23
*****
FLOW PROCESS FROM NODE      185.00 TO NODE      186.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    485.25
DOWNSTREAM ELEVATION(FEET) =    484.60
ELEVATION DIFFERENCE(FEET) =    0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =    5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
         THE MAXIMUM OVERLAND FLOW LENGTH =    65.00
         (Reference: Table 3-1B of Hydrology Manual)
         THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  5.555
SUBAREA RUNOFF(CFS) =    0.79
TOTAL AREA(ACRES) =    0.19  TOTAL RUNOFF(CFS) =    0.79
*****
FLOW PROCESS FROM NODE      186.00 TO NODE      187.00 IS CODE =  61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STANDARD CURB SECTION USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  484.60  DOWNSTREAM ELEVATION(FEET) =  430.00
STREET LENGTH(FEET) =   524.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =   16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    8.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    5.22
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.24
HALFSTREET FLOOD WIDTH(FEET) =    5.84
AVERAGE FLOW VELOCITY(FEET/SEC.) =    5.68
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.38
STREET FLOW TRAVEL TIME(MIN.) =    1.54  Tc(MIN.) =    6.62
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.684
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500

```

AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.51 SUBAREA RUNOFF(CFS) = 8.82  
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 9.49

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.87  
FLOW VELOCITY(FEET/SEC.) = 6.43 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.82  
LONGEST FLOWPATH FROM NODE 185.00 TO NODE 187.00 = 589.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 187.00 TO NODE 187.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	6.62
RAINFALL INTENSITY(INCH/HR) =	4.68
TOTAL STREAM AREA(ACRES) =	2.70
PEAK FLOW RATE(CFS) AT CONFLUENCE =	9.49

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	28.23	8.49	3.989	11.24
2	9.49	6.62	4.684	2.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	33.52	6.62	4.684
2	36.30	8.49	3.989

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 36.30 Tc(MIN.) = 8.49  
TOTAL AREA(ACRES) = 13.9  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 187.00 = 1738.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 187.00 TO NODE 192.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	425.00	DOWNSTREAM(FEET) =	418.00
FLOW LENGTH(FEET) =	575.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS	21.2	INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.81		
ESTIMATED PIPE DIAMETER(INCH) =	30.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	36.30		
PIPE TRAVEL TIME(MIN.) =	0.98	Tc(MIN.) =	9.46
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 192.00 =	2313.00	FEET.	

\*\*\*\*\*  
FLOW PROCESS FROM NODE 192.00 TO NODE 192.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.46
RAINFALL INTENSITY(INCH/HR) =	3.72
TOTAL STREAM AREA(ACRES) =	13.94
PEAK FLOW RATE(CFS) AT CONFLUENCE =	36.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 190.00 TO NODE 191.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 434.55  
 DOWNSTREAM ELEVATION(FEET) = 433.90  
 ELEVATION DIFFERENCE(FEET) = 0.65  
 URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.555  
 SUBAREA RUNOFF(CFS) = 0.33  
 TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.33

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 191.00 TO NODE 192.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 433.90 DOWNSTREAM ELEVATION(FEET) = 423.00  
 STREET LENGTH(FEET) = 681.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.07  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.34  
 HALFSTREET FLOOD WIDTH(FEET) = 10.47  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.91  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.98  
 STREET FLOW TRAVEL TIME(MIN.) = 3.90 Tc(MIN.) = 8.98  
 50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.847  
 \*USER SPECIFIED(SUBAREA):  
 DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
 SUBAREA AREA(ACRES) = 4.57 SUBAREA RUNOFF(CFS) = 13.19  
 TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 13.42

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.66  
 FLOW VELOCITY(FEET/SEC.) = 3.38 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.35  
 LONGEST FLOWPATH FROM NODE 190.00 TO NODE 192.00 = 746.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 192.00 TO NODE 192.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.98  
 RAINFALL INTENSITY(INCH/HR) = 3.85  
 TOTAL STREAM AREA(ACRES) = 4.65  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	36.30	9.46	3.719	13.94
2	13.42	8.98	3.847	4.65

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	36.30	9.46	3.719
2	13.42	8.98	3.847

1 48.51 8.98 3.847  
2 49.27 9.46 3.719

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 49.27 Tc(MIN.) = 9.46  
TOTAL AREA(ACRES) = 18.6  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 192.00 = 2313.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 192.00 TO NODE 162.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 418.00 DOWNSTREAM(FEET) = 362.00  
FLOW LENGTH(FEET) = 539.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.91  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 49.27  
PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 9.84  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 162.00 = 2852.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	49.27	9.84	3.626	18.59

LONGEST FLOWPATH FROM NODE 170.00 TO NODE 162.00 = 2852.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	117.07	10.15	3.555	42.97

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	162.77	9.84	3.626
2	165.36	10.15	3.555

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 165.36 Tc(MIN.) = 10.15  
TOTAL AREA(ACRES) = 61.6

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 197.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 362.00 DOWNSTREAM(FEET) = 315.00  
FLOW LENGTH(FEET) = 915.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.31  
ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 165.36  
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 10.78  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 197.00 = 4351.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.78
RAINFALL INTENSITY(INCH/HR) = 3.42
TOTAL STREAM AREA(ACRES) = 61.56
PEAK FLOW RATE(CFS) AT CONFLUENCE = 165.36

*****
FLOW PROCESS FROM NODE 195.00 TO NODE 196.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .7300
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 370.00
DOWNSTREAM ELEVATION(FEET) = 360.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.092
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.52
TOTAL AREA(ACRES) = 0.37 TOTAL RUNOFF(CFS) = 1.52

*****
FLOW PROCESS FROM NODE 196.00 TO NODE 197.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 360.60 DOWNSTREAM ELEVATION(FEET) = 318.50
STREET LENGTH(FEET) = 805.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 22.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.61
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 9.63
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.08
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.62
STREET FLOW TRAVEL TIME(MIN.) = 2.64 Tc(MIN.) = 5.73
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.137
*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .7200
AREA-AVERAGE RUNOFF COEFFICIENT = 0.721
SUBAREA AREA(ACRES) = 4.90 SUBAREA RUNOFF(CFS) = 18.12
TOTAL AREA(ACRES) = 5.3 PEAK FLOW RATE(CFS) = 19.51

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.51
FLOW VELOCITY(FEET/SEC.) = 5.80 DEPTH*VELOCITY(FT*FT/SEC.) = 2.18
LONGEST FLOWPATH FROM NODE 195.00 TO NODE 197.00 = 905.00 FEET.

*****
FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.73
RAINFALL INTENSITY(INCH/HR) = 5.14
TOTAL STREAM AREA(ACRES) = 5.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.51

```



\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	165.36	10.78	3.420	61.56
2	19.51	5.73	5.137	5.27

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	107.51	5.73	5.137
2	178.35	10.78	3.420

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 178.35 Tc(MIN.) = 10.78  
TOTAL AREA(ACRES) = 66.8  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 197.00 = 4351.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 313.00 DOWNSTREAM(FEET) = 283.50  
FLOW LENGTH(FEET) = 858.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 45.0 INCH PIPE IS 31.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.57  
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 178.35  
PIPE TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 11.44  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 198.00 = 5209.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.291  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (HILLY) RUNOFF COEFFICIENT = .5000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7261  
SUBAREA AREA(ACRES) = 2.15 SUBAREA RUNOFF(CFS) = 3.54  
TOTAL AREA(ACRES) = 69.0 TOTAL RUNOFF(CFS) = 178.35  
TC(MIN.) = 11.44  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 198.00 TO NODE 198.00 IS CODE = 7  
-----

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<  
=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 22.24 RAIN INTENSITY(INCH/HOUR) = 2.14  
TOTAL AREA(ACRES) = 68.98 TOTAL RUNOFF(CFS) = 83.92

\*\*\*\*\*  
FLOW PROCESS FROM NODE 198.00 TO NODE 304.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 278.00 DOWNSTREAM(FEET) = 200.00  
FLOW LENGTH(FEET) = 1006.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 24.38  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 83.92  
PIPE TRAVEL TIME(MIN.) = 0.69 Tc(MIN.) = 22.93  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 304.00 = 6215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1  
-----

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 22.93
RAINFALL INTENSITY(INCH/HR) = 2.10
TOTAL STREAM AREA(ACRES) = 68.98
PEAK FLOW RATE(CFS) AT CONFLUENCE = 83.92

*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 655.00
DOWNSTREAM ELEVATION(FEET) = 645.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.612
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.11
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.11

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 645.00 DOWNSTREAM(FEET) = 450.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1066.00 CHANNEL SLOPE = 0.1829
CHANNEL FLOW THRU SUBAREA(CFS) = 1.11
FLOW VELOCITY(FEET/SEC) = 2.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 7.16 Tc(MIN.) = 11.34
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1166.00 FEET.

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.309
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 18.82 SUBAREA RUNOFF(CFS) = 37.37
TOTAL AREA(ACRES) = 19.1 TOTAL RUNOFF(CFS) = 38.02
TC(MIN.) = 11.34

*****
FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 305.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2180.00 CHANNEL SLOPE = 0.0665
CHANNEL FLOW THRU SUBAREA(CFS) = 38.02
FLOW VELOCITY(FEET/SEC) = 9.23 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.94 Tc(MIN.) = 15.28
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 3346.00 FEET.

*****
FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.731
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000

```

SUBAREA AREA(ACRES) = 34.79 SUBAREA RUNOFF(CFS) = 57.00  
TOTAL AREA(ACRES) = 53.9 TOTAL RUNOFF(CFS) = 88.38  
TC(MIN.) = 15.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	305.00	DOWNSTREAM(FEET) =	200.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	751.00	CHANNEL SLOPE =	0.1398
CHANNEL FLOW THRU SUBAREA(CFS) =	88.38		
FLOW VELOCITY(FEET/SEC) =	9.31	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	1.34	Tc(MIN.) =	16.62
LONGEST FLOWPATH FROM NODE	300.00 TO NODE	304.00 =	4097.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.586		
*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000		
SUBAREA AREA(ACRES) =	4.88	SUBAREA RUNOFF(CFS) =	7.57
TOTAL AREA(ACRES) =	58.8	TOTAL RUNOFF(CFS) =	91.27
TC(MIN.) =	16.62		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	16.62
RAINFALL INTENSITY(INCH/HR) =	2.59
TOTAL STREAM AREA(ACRES) =	58.82
PEAK FLOW RATE(CFS) AT CONFLUENCE =	91.27

\*\*\*\*\*  
FLOW PROCESS FROM NODE 310.00 TO NODE 311.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00		
UPSTREAM ELEVATION(FEET) =	410.00		
DOWNSTREAM ELEVATION(FEET) =	400.00		
ELEVATION DIFFERENCE(FEET) =	10.00		
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178		
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!			
50 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.612		
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.			
SUBAREA RUNOFF(CFS) =	2.16		
TOTAL AREA(ACRES) =	0.64	TOTAL RUNOFF(CFS) =	2.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	400.00	DOWNSTREAM(FEET) =	264.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	2121.00	CHANNEL SLOPE =	0.0641
CHANNEL FLOW THRU SUBAREA(CFS) =	2.16		
FLOW VELOCITY(FEET/SEC) =	4.43	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	7.99	Tc(MIN.) =	12.16
LONGEST FLOWPATH FROM NODE	310.00 TO NODE	312.00 =	2221.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 81  
-----

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.163
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 28.42 SUBAREA RUNOFF(CFS) = 53.94
TOTAL AREA(ACRES) = 29.1 TOTAL RUNOFF(CFS) = 55.15
TC(MIN.) = 12.16
*****
FLOW PROCESS FROM NODE 312.00 TO NODE 313.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 224.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1340.00 CHANNEL SLOPE = 0.0299
CHANNEL FLOW THRU SUBAREA(CFS) = 55.15
FLOW VELOCITY(FEET/SEC) = 6.88 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.25 Tc(MIN.) = 15.41
LONGEST FLOWPATH FROM NODE 310.00 TO NODE 313.00 = 3561.00 FEET.
*****
FLOW PROCESS FROM NODE 312.00 TO NODE 313.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.715
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 27.10 SUBAREA RUNOFF(CFS) = 44.15
TOTAL AREA(ACRES) = 56.2 TOTAL RUNOFF(CFS) = 91.50
TC(MIN.) = 15.41
*****
FLOW PROCESS FROM NODE 313.00 TO NODE 304.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 224.00 DOWNSTREAM(FEET) = 200.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1435.00 CHANNEL SLOPE = 0.0167
CHANNEL FLOW THRU SUBAREA(CFS) = 91.50
FLOW VELOCITY(FEET/SEC) = 5.98 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 4.00 Tc(MIN.) = 19.41
LONGEST FLOWPATH FROM NODE 310.00 TO NODE 304.00 = 4996.00 FEET.
*****
FLOW PROCESS FROM NODE 313.00 TO NODE 304.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
50 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.340
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 19.13 SUBAREA RUNOFF(CFS) = 26.86
TOTAL AREA(ACRES) = 75.3 TOTAL RUNOFF(CFS) = 105.70
TC(MIN.) = 19.41
*****
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 19.41
RAINFALL INTENSITY(INCH/HR) = 2.34
TOTAL STREAM AREA(ACRES) = 75.29
PEAK FLOW RATE(CFS) AT CONFLUENCE = 105.70

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	83.92	22.93	2.101	68.98
2	91.27	16.62	2.586	58.82
3	105.70	19.41	2.340	75.29

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	242.60	16.62	2.586
2	259.32	19.41	2.340
3	253.02	22.93	2.101

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 259.32 Tc(MIN.) = 19.41  
 TOTAL AREA(ACRES) = 203.1  
 LONGEST FLOWPATH FROM NODE 110.00 TO NODE 304.00 = 6215.00 FEET.

=====  
 END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 203.1 TC(MIN.) = 19.41  
 PEAK FLOW RATE(CFS) = 259.32  
 =====

END OF RATIONAL METHOD ANALYSIS

## **CHAPTER 3**

### **HYDROLOGIC ANALYSIS**

#### **3.4 – 100-Year Developed Condition AES Model Output**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2015 Advanced Engineering Software (aes)
Ver. 22.0 Release Date: 07/01/2015 License ID 1239

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*
\* Otay Ranch Village 4 South \*
\* 100-year return interval: Proposed Condition \*
\* DLN 0924, W.O. 3206-0002 \*
\*\*\*\*\*

FILE NAME: R:\0924\HYD\CALCS\AES\PR100.DAT
TIME/DATE OF STUDY: 12:45 06/22/2016

-----
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00
6-HOUR DURATION PRECIPITATION (INCHES) = 2.350
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*
Table with 10 columns: NO., HALF-WIDTH (FT), CROWN CROSSFALL (FT), STREET-CROSSFALL IN-/OUT-/SIDE, PARK-/WAY, CURB HEIGHT (FT), GUTTER WIDTH (FT), GEOMETRIES LIP (FT), HIKE (FT), MANNING FACTOR (n). Rows 1-6.

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.50 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .8500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00
UPSTREAM ELEVATION(FEET) = 437.63
DOWNSTREAM ELEVATION(FEET) = 437.02
ELEVATION DIFFERENCE(FEET) = 0.61
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.467
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 2.16
TOTAL AREA(ACRES) = 0.41 TOTAL RUNOFF(CFS) = 2.16

\*\*\*\*\*
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 62
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 6 USED)<<<<

=====
UPSTREAM ELEVATION(FEET) = 437.02 DOWNSTREAM ELEVATION(FEET) = 432.91
STREET LENGTH(FEET) = 413.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 12.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0150

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.47
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.29
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.77
STREET FLOW TRAVEL TIME(MIN.) = 3.01 Tc(MIN.) = 6.48
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.240
\*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .8500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
SUBAREA AREA(ACRES) = 1.51 SUBAREA RUNOFF(CFS) = 6.73
TOTAL AREA(ACRES) = 1.9 PEAK FLOW RATE(CFS) = 8.55

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.49
FLOW VELOCITY(FEET/SEC.) = 2.55 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.96
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 473.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 428.00 DOWNSTREAM(FEET) = 427.00
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.36
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.55
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 6.58
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 523.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====

\*\*\*\*\*
FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
\*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 525.00
DOWNSTREAM ELEVATION(FEET) = 515.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.11 TOTAL RUNOFF(CFS) = 0.41

\*\*\*\*\*
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 31
=====



>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 515.00 DOWNSTREAM(FEET) = 451.00  
FLOW LENGTH(FEET) = 548.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.55  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.41  
PIPE TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 5.57  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 648.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.774  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000  
SUBAREA AREA(ACRES) = 2.16 SUBAREA RUNOFF(CFS) = 7.48  
TOTAL AREA(ACRES) = 2.3 TOTAL RUNOFF(CFS) = 7.86  
TC(MIN.) = 5.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 112.00 TO NODE 117.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 446.00 DOWNSTREAM(FEET) = 435.00  
FLOW LENGTH(FEET) = 254.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.93  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.86  
PIPE TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 5.96  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 117.00 = 902.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.96  
RAINFALL INTENSITY(INCH/HR) = 5.53  
TOTAL STREAM AREA(ACRES) = 2.27  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.86

\*\*\*\*\*  
FLOW PROCESS FROM NODE 115.00 TO NODE 116.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 526.45  
DOWNSTREAM ELEVATION(FEET) = 525.80  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 1.24  
TOTAL AREA(ACRES) = 0.27 TOTAL RUNOFF(CFS) = 1.24

\*\*\*\*\*  
FLOW PROCESS FROM NODE 116.00 TO NODE 117.00 IS CODE = 61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 525.80 DOWNSTREAM ELEVATION(FEET) = 438.25  
STREET LENGTH(FEET) = 721.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.41  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.57  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.81  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.89  
STREET FLOW TRAVEL TIME(MIN.) = 1.77 Tc(MIN.) = 6.84  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.057  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 4.28 SUBAREA RUNOFF(CFS) = 16.23  
TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 17.26

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 9.97  
FLOW VELOCITY(FEET/SEC.) = 7.76 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.53  
LONGEST FLOWPATH FROM NODE 115.00 TO NODE 117.00 = 786.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 117.00 TO NODE 117.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.84  
RAINFALL INTENSITY(INCH/HR) = 5.06  
TOTAL STREAM AREA(ACRES) = 4.55  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.26

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.86	5.96	5.529	2.27
2	17.26	6.84	5.057	4.55

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	22.89	5.96	5.529
2	24.45	6.84	5.057

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 24.45 Tc(MIN.) = 6.84  
TOTAL AREA(ACRES) = 6.8  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 117.00 = 902.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 117.00 TO NODE 118.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 433.00 DOWNSTREAM(FEET) = 427.00  
FLOW LENGTH(FEET) = 272.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.18  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 24.45  
PIPE TRAVEL TIME(MIN.) = 0.41 Tc(MIN.) = 7.25  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 118.00 = 1174.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 118.00 TO NODE 118.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
-----  
TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.25  
RAINFALL INTENSITY(INCH/HR) = 4.87  
TOTAL STREAM AREA(ACRES) = 6.82  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 24.45

\*\*\*\*\*  
FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
-----  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 451.55  
DOWNSTREAM ELEVATION(FEET) = 450.90  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 1.43  
TOTAL AREA(ACRES) = 0.31 TOTAL RUNOFF(CFS) = 1.43

\*\*\*\*\*  
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
-----  
UPSTREAM ELEVATION(FEET) = 446.20 DOWNSTREAM ELEVATION(FEET) = 430.50  
STREET LENGTH(FEET) = 446.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00  
  
DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.78  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.66  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.91  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.17  
STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 6.98  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.992  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.84 SUBAREA RUNOFF(CFS) = 10.63  
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 11.79

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.03  
FLOW VELOCITY(FEET/SEC.) = 4.42 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.53  
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 122.00 = 511.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 81

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-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.992
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (HILLY) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7402
SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.66
TOTAL AREA(ACRES) = 3.4 TOTAL RUNOFF(CFS) = 12.45
TC(MIN.) = 6.98

*****
FLOW PROCESS FROM NODE 122.00 TO NODE 118.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.98
RAINFALL INTENSITY(INCH/HR) = 4.99
TOTAL STREAM AREA(ACRES) = 3.37
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.45

*****
FLOW PROCESS FROM NODE 125.00 TO NODE 126.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 453.85
DOWNSTREAM ELEVATION(FEET) = 453.20
ELEVATION DIFFERENCE(FEET) = 0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129
SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 0.09 TOTAL RUNOFF(CFS) = 0.41

*****
FLOW PROCESS FROM NODE 126.00 TO NODE 127.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 453.20 DOWNSTREAM ELEVATION(FEET) = 430.50
STREET LENGTH(FEET) = 655.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.74
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.29
HALFSTREET FLOOD WIDTH(FEET) = 8.03
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.76
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.08
STREET FLOW TRAVEL TIME(MIN.) = 2.90 Tc(MIN.) = 7.98
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.579
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750
SUBAREA AREA(ACRES) = 3.06 SUBAREA RUNOFF(CFS) = 10.51
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 10.82

```

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.66  
 FLOW VELOCITY(FEET/SEC.) = 4.31 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.46  
 LONGEST FLOWPATH FROM NODE 125.00 TO NODE 127.00 = 720.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 127.00 TO NODE 118.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.98  
 RAINFALL INTENSITY(INCH/HR) = 4.58  
 TOTAL STREAM AREA(ACRES) = 3.15  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.82

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	24.45	7.25	4.872	6.82
2	12.45	6.98	4.992	3.37
3	10.82	7.98	4.579	3.15

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	45.78	6.98	4.992
2	46.43	7.25	4.872
3	45.22	7.98	4.579

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 46.43 Tc(MIN.) = 7.25  
 TOTAL AREA(ACRES) = 13.3  
 LONGEST FLOWPATH FROM NODE 110.00 TO NODE 118.00 = 1174.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 118.00 TO NODE 103.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 427.00 DOWNSTREAM(FEET) = 426.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.79  
 ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 46.43  
 PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 7.50  
 LONGEST FLOWPATH FROM NODE 110.00 TO NODE 103.00 = 1304.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 130.00 TO NODE 130.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	46.43	7.50	4.768	13.34

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 130.00 = 1304.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.55	6.58	5.189	1.92

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 130.00 = 523.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
---------------	--------------	-----------	-----------------------

1 49.28 6.58 5.189  
2 54.29 7.50 4.768

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 54.29 Tc(MIN.) = 7.50  
TOTAL AREA(ACRES) = 15.3

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 12  
-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 128.00 IS CODE = 31  
-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 426.00 DOWNSTREAM(FEET) = 422.00  
FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.47  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 54.29  
PIPE TRAVEL TIME(MIN.) = 0.81 Tc(MIN.) = 8.31  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 128.00 = 1764.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 128.00 TO NODE 128.00 IS CODE = 1  
-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.31  
RAINFALL INTENSITY(INCH/HR) = 4.46  
TOTAL STREAM AREA(ACRES) = 15.26  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 54.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 444.15  
DOWNSTREAM ELEVATION(FEET) = 443.50  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 0.46  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 31  
-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 435.80 DOWNSTREAM(FEET) = 428.00  
FLOW LENGTH(FEET) = 995.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.64  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.46  
PIPE TRAVEL TIME(MIN.) = 6.29 Tc(MIN.) = 11.37  
LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 1060.00 FEET.

```

*****
FLOW PROCESS FROM NODE      131.00 TO NODE      132.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.645
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7500
SUBAREA AREA(ACRES) =      6.96  SUBAREA RUNOFF(CFS) =    19.03
TOTAL AREA(ACRES) =      7.1  TOTAL RUNOFF(CFS) =    19.30
TC(MIN.) =    11.37

*****
FLOW PROCESS FROM NODE      132.00 TO NODE      128.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  438.50  DOWNSTREAM(FEET) =  422.00
FLOW LENGTH(FEET) =  115.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  9.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  21.48
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =    19.30
PIPE TRAVEL TIME(MIN.) =  0.09  Tc(MIN.) =  11.46
LONGEST FLOWPATH FROM NODE      130.00 TO NODE      128.00 =    1175.00 FEET.

*****
FLOW PROCESS FROM NODE      128.00 TO NODE      128.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =  11.46
RAINFALL INTENSITY(INCH/HR) =  3.63
TOTAL STREAM AREA(ACRES) =  7.06
PEAK FLOW RATE(CFS) AT CONFLUENCE =    19.30

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)  (ACRE)
1           54.29      8.31      4.463      15.26
2           19.30     11.46      3.627      7.06

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR  2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
1           68.28      8.31      4.463
2           63.42     11.46      3.627

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =    68.28  Tc(MIN.) =    8.31
TOTAL AREA(ACRES) =    22.3
LONGEST FLOWPATH FROM NODE      110.00 TO NODE      128.00 =    1764.00 FEET.

*****
FLOW PROCESS FROM NODE      128.00 TO NODE      137.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  422.00  DOWNSTREAM(FEET) =  414.00
FLOW LENGTH(FEET) =  610.00  MANNING'S N =  0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  11.66
ESTIMATED PIPE DIAMETER(INCH) =  36.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =    68.28
PIPE TRAVEL TIME(MIN.) =  0.87  Tc(MIN.) =    9.18
LONGEST FLOWPATH FROM NODE      110.00 TO NODE      137.00 =    2374.00 FEET.

```

\*\*\*\*\*  
FLOW PROCESS FROM NODE 137.00 TO NODE 137.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.18
RAINFALL INTENSITY(INCH/HR) =	4.18
TOTAL STREAM AREA(ACRES) =	22.32
PEAK FLOW RATE(CFS) AT CONFLUENCE =	68.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 135.00 TO NODE 136.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

PAVED SURFACE RUNOFF COEFFICIENT =	.8500
INITIAL SUBAREA FLOW-LENGTH(FEET) =	103.00
UPSTREAM ELEVATION(FEET) =	432.50
DOWNSTREAM ELEVATION(FEET) =	431.60
ELEVATION DIFFERENCE(FEET) =	0.90
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	3.568

WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 57.48  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.	
SUBAREA RUNOFF(CFS) =	1.32
TOTAL AREA(ACRES) =	0.25
TOTAL RUNOFF(CFS) =	1.32

\*\*\*\*\*  
FLOW PROCESS FROM NODE 136.00 TO NODE 137.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	430.75	DOWNSTREAM ELEVATION(FEET) =	418.50
STREET LENGTH(FEET) =	1000.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	44.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	22.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	2
STREET PARKWAY CROSSFALL(DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =	0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	9.02
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:	
STREET FLOW DEPTH(FEET) =	0.37
HALFSTREET FLOOD WIDTH(FEET) =	12.27
AVERAGE FLOW VELOCITY(FEET/SEC.) =	2.78
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =	1.03
STREET FLOW TRAVEL TIME(MIN.) =	6.00
Tc(MIN.) =	9.57
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	4.073

\*USER SPECIFIED(SUBAREA):

COMMERCIAL AREA RUNOFF COEFFICIENT =	.8500
AREA-AVERAGE RUNOFF COEFFICIENT =	0.850
SUBAREA AREA(ACRES) =	4.30
SUBAREA RUNOFF(CFS) =	14.89
TOTAL AREA(ACRES) =	4.6
PEAK FLOW RATE(CFS) =	15.75

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) =	0.43	HALFSTREET FLOOD WIDTH(FEET) =	15.31	
FLOW VELOCITY(FEET/SEC.) =	3.20	DEPTH*VELOCITY(FT*FT/SEC.) =	1.38	
LONGEST FLOWPATH FROM NODE	135.00	TO NODE	137.00 =	1103.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 137.00 TO NODE 137.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<



```

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.57
RAINFALL INTENSITY(INCH/HR) = 4.07
TOTAL STREAM AREA(ACRES) = 4.55
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.75

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
1           68.28      9.18    4.185          22.32
2           15.75      9.57    4.073          4.55

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
1           83.38      9.18    4.185
2           82.21      9.57    4.073

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 83.38   Tc(MIN.) = 9.18
TOTAL AREA(ACRES) = 26.9
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 137.00 = 2374.00 FEET.

*****
FLOW PROCESS FROM NODE 137.00 TO NODE 138.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 412.00  DOWNSTREAM(FEET) = 411.00
FLOW LENGTH(FEET) = 75.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.37
ESTIMATED PIPE DIAMETER(INCH) = 39.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 83.38
PIPE TRAVEL TIME(MIN.) = 0.10  Tc(MIN.) = 9.28
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 138.00 = 2449.00 FEET.

*****
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====
*****
FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 460.00
DOWNSTREAM ELEVATION(FEET) = 450.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.74
TOTAL AREA(ACRES) = 0.20  TOTAL RUNOFF(CFS) = 0.74

*****
FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 450.00  DOWNSTREAM(FEET) = 425.00
FLOW LENGTH(FEET) = 652.00  MANNING'S N = 0.013

```

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ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.31
ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.74
PIPE TRAVEL TIME(MIN.) = 2.05    Tc(MIN.) = 6.23
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 142.00 = 752.00 FEET.

*****
FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.375
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 2.56    SUBAREA RUNOFF(CFS) = 8.26
TOTAL AREA(ACRES) = 2.8    TOTAL RUNOFF(CFS) = 8.90
TC(MIN.) = 6.23

*****
FLOW PROCESS FROM NODE 142.00 TO NODE 147.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 420.00    DOWNSTREAM(FEET) = 417.00
FLOW LENGTH(FEET) = 271.00    MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.66
ESTIMATED PIPE DIAMETER(INCH) = 18.00    NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.90
PIPE TRAVEL TIME(MIN.) = 0.68    Tc(MIN.) = 6.90
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 147.00 = 1023.00 FEET.

*****
FLOW PROCESS FROM NODE 147.00 TO NODE 147.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.90
RAINFALL INTENSITY(INCH/HR) = 5.03
TOTAL STREAM AREA(ACRES) = 2.76
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.90

*****
FLOW PROCESS FROM NODE 145.00 TO NODE 146.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 449.15
DOWNSTREAM ELEVATION(FEET) = 448.50
ELEVATION DIFFERENCE(FEET) = 0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH = 65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129
SUBAREA RUNOFF(CFS) = 0.51
TOTAL AREA(ACRES) = 0.11    TOTAL RUNOFF(CFS) = 0.51

*****
FLOW PROCESS FROM NODE 146.00 TO NODE 147.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 448.50    DOWNSTREAM ELEVATION(FEET) = 421.50
STREET LENGTH(FEET) = 614.00    CURB HEIGHT(INCHES) = 6.0

```

STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.86  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 7.67  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.15  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.16  
STREET FLOW TRAVEL TIME(MIN.) = 2.47 Tc(MIN.) = 7.55  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.748  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.98 SUBAREA RUNOFF(CFS) = 10.61  
TOTAL AREA(ACRES) = 3.1 PEAK FLOW RATE(CFS) = 11.00

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 10.22  
FLOW VELOCITY(FEET/SEC.) = 4.73 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.57  
LONGEST FLOWPATH FROM NODE 145.00 TO NODE 147.00 = 679.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 147.00 TO NODE 147.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.55  
RAINFALL INTENSITY(INCH/HR) = 4.75  
TOTAL STREAM AREA(ACRES) = 3.09  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.00

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.90	6.90	5.029	2.76
2	11.00	7.55	4.748	3.09

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	18.97	6.90	5.029
2	19.41	7.55	4.748

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 19.41 Tc(MIN.) = 7.55  
TOTAL AREA(ACRES) = 5.8  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 147.00 = 1023.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 147.00 TO NODE 148.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 417.00 DOWNSTREAM(FEET) = 411.00  
FLOW LENGTH(FEET) = 192.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.06  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 19.41  
PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 7.81

```

LONGEST FLOWPATH FROM NODE    140.00 TO NODE    148.00 =    1215.00 FEET.
*****
FLOW PROCESS FROM NODE    148.00 TO NODE    148.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    7.81
RAINFALL INTENSITY(INCH/HR) =    4.64
TOTAL STREAM AREA(ACRES) =    5.85
PEAK FLOW RATE(CFS) AT CONFLUENCE =    19.41
*****
FLOW PROCESS FROM NODE    150.00 TO NODE    151.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    453.45
DOWNSTREAM ELEVATION(FEET) =    452.80
ELEVATION DIFFERENCE(FEET) =    0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =    5.079
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    6.129
SUBAREA RUNOFF(CFS) =    0.46
TOTAL AREA(ACRES) =    0.10  TOTAL RUNOFF(CFS) =    0.46
*****
FLOW PROCESS FROM NODE    151.00 TO NODE    152.00 IS CODE =    61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =    452.80  DOWNSTREAM ELEVATION(FEET) =    415.80
STREET LENGTH(FEET) =    900.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    8.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =    0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    6.03
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.28
HALFSTREET FLOOD WIDTH(FEET) =    7.92
AVERAGE FLOW VELOCITY(FEET/SEC.) =    4.04
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.15
STREET FLOW TRAVEL TIME(MIN.) =    3.71  Tc(MIN.) =    8.79
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    4.302
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
AREA-AVERAGE RUNOFF COEFFICIENT =    0.750
SUBAREA AREA(ACRES) =    3.39  SUBAREA RUNOFF(CFS) =    10.94
TOTAL AREA(ACRES) =    3.5  PEAK FLOW RATE(CFS) =    11.26

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =    0.34  HALFSTREET FLOOD WIDTH(FEET) =    10.47
FLOW VELOCITY(FEET/SEC.) =    4.64  DEPTH*VELOCITY(FT*FT/SEC.) =    1.56
LONGEST FLOWPATH FROM NODE    150.00 TO NODE    152.00 =    965.00 FEET.
*****
FLOW PROCESS FROM NODE    152.00 TO NODE    148.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
TIME OF CONCENTRATION(MIN.) =    8.79

```

RAINFALL INTENSITY(INCH/HR) = 4.30  
TOTAL STREAM AREA(ACRES) = 3.49  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.26

\*\*\*\*\*  
FLOW PROCESS FROM NODE 155.00 TO NODE 156.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 430.25  
DOWNSTREAM ELEVATION(FEET) = 429.60  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 0.46  
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 156.00 TO NODE 157.00 IS CODE = 61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 429.60 DOWNSTREAM ELEVATION(FEET) = 415.80  
STREET LENGTH(FEET) = 476.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.58  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.24  
HALFSTREET FLOOD WIDTH(FEET) = 5.64  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.96  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
STREET FLOW TRAVEL TIME(MIN.) = 2.68 Tc(MIN.) = 7.76  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.662

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 4.20  
TOTAL AREA(ACRES) = 1.3 PEAK FLOW RATE(CFS) = 4.55

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 7.52  
FLOW VELOCITY(FEET/SEC.) = 3.33 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.92  
LONGEST FLOWPATH FROM NODE 155.00 TO NODE 157.00 = 541.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 157.00 TO NODE 148.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.76  
RAINFALL INTENSITY(INCH/HR) = 4.66  
TOTAL STREAM AREA(ACRES) = 1.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.55

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.41	7.81	4.644	5.85
2	11.26	8.79	4.302	3.49
3	4.55	7.76	4.662	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	33.82	7.76	4.662
2	33.94	7.81	4.644
3	33.44	8.79	4.302

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 33.94 Tc(MIN.) = 7.81  
TOTAL AREA(ACRES) = 10.6  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 148.00 = 1215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 148.00 TO NODE 138.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 411.00 DOWNSTREAM(FEET) = 410.00  
FLOW LENGTH(FEET) = 122.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.17  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 33.94  
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 8.06  
LONGEST FLOWPATH FROM NODE 140.00 TO NODE 138.00 = 1337.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	33.94	8.06	4.551	10.64

LONGEST FLOWPATH FROM NODE 140.00 TO NODE 138.00 = 1337.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	83.38	9.28	4.155	26.87

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 138.00 = 2449.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	106.36	8.06	4.551
2	114.38	9.28	4.155

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 114.38 Tc(MIN.) = 9.28  
TOTAL AREA(ACRES) = 37.5

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 138.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 138.00 TO NODE 162.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 411.00 DOWNSTREAM(FEET) = 362.00  
FLOW LENGTH(FEET) = 987.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 24.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.21  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 114.38  
PIPE TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 10.02  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.02  
RAINFALL INTENSITY(INCH/HR) = 3.95  
TOTAL STREAM AREA(ACRES) = 37.51  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 114.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 160.00 TO NODE 161.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
PAVED SURFACE RUNOFF COEFFICIENT = .8500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 419.00  
DOWNSTREAM ELEVATION(FEET) = 415.50  
ELEVATION DIFFERENCE(FEET) = 3.50  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.692  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 82.50  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.21  
TOTAL AREA(ACRES) = 0.23 TOTAL RUNOFF(CFS) = 1.21

\*\*\*\*\*

FLOW PROCESS FROM NODE 161.00 TO NODE 162.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 415.50 DOWNSTREAM ELEVATION(FEET) = 367.00  
STREET LENGTH(FEET) = 928.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 22.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.12  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.33  
HALFSTREET FLOOD WIDTH(FEET) = 10.27  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.17  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.71  
STREET FLOW TRAVEL TIME(MIN.) = 2.99 Tc(MIN.) = 5.68  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.700  
\*USER SPECIFIED(SUBAREA):  
PAVED SURFACE RUNOFF COEFFICIENT = .7200  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.725  
SUBAREA AREA(ACRES) = 5.23 SUBAREA RUNOFF(CFS) = 21.46  
TOTAL AREA(ACRES) = 5.5 PEAK FLOW RATE(CFS) = 22.58

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.23  
FLOW VELOCITY(FEET/SEC.) = 6.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.36  
LONGEST FLOWPATH FROM NODE 160.00 TO NODE 162.00 = 1028.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	5.68
RAINFALL INTENSITY(INCH/HR) =	5.70
TOTAL STREAM AREA(ACRES) =	5.46
PEAK FLOW RATE(CFS) AT CONFLUENCE =	22.58

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	114.38	10.02	3.955	37.51
2	22.58	5.68	5.700	5.46

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	87.47	5.68	5.700
2	130.04	10.02	3.955

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 130.04 Tc(MIN.) = 10.02  
TOTAL AREA(ACRES) = 43.0  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 170.00 TO NODE 171.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 556.05  
DOWNSTREAM ELEVATION(FEET) = 555.40  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
(Reference: Table 3-1B of Hydrology Manual)  
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 0.83  
TOTAL AREA(ACRES) = 0.18 TOTAL RUNOFF(CFS) = 0.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 171.00 TO NODE 172.00 IS CODE = 61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	555.40	DOWNSTREAM ELEVATION(FEET) =	529.00
STREET LENGTH(FEET) =	620.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	16.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020



SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.75  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.78  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.36  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.32  
STREET FLOW TRAVEL TIME(MIN.) = 2.37 Tc(MIN.) = 7.45  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.787  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 3.82 SUBAREA RUNOFF(CFS) = 13.72  
TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 14.36

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.47  
FLOW VELOCITY(FEET/SEC.) = 5.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.78  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 172.00 = 685.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 172.00 TO NODE 177.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 524.00 DOWNSTREAM(FEET) = 479.00  
FLOW LENGTH(FEET) = 483.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.96  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.36  
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 7.92  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 177.00 = 1168.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.92  
RAINFALL INTENSITY(INCH/HR) = 4.60  
TOTAL STREAM AREA(ACRES) = 4.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.36

\*\*\*\*\*  
FLOW PROCESS FROM NODE 175.00 TO NODE 176.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 529.95  
DOWNSTREAM ELEVATION(FEET) = 529.30  
ELEVATION DIFFERENCE(FEET) = 0.65  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
SUBAREA RUNOFF(CFS) = 0.74  
TOTAL AREA(ACRES) = 0.16 TOTAL RUNOFF(CFS) = 0.74

\*\*\*\*\*  
FLOW PROCESS FROM NODE 176.00 TO NODE 177.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 529.30 DOWNSTREAM ELEVATION(FEET) = 484.00

STREET LENGTH(FEET) = 424.70 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 16.00  
  
DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020  
  
SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.78  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 6.15  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.83  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.45  
STREET FLOW TRAVEL TIME(MIN.) = 1.21 Tc(MIN.) = 6.29  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.337  
\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.51 SUBAREA RUNOFF(CFS) = 10.05  
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 10.69

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.28  
FLOW VELOCITY(FEET/SEC.) = 6.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.94  
LONGEST FLOWPATH FROM NODE 175.00 TO NODE 177.00 = 489.70 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 177.00 TO NODE 177.00 IS CODE = 1  
-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
-----  
TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.29  
RAINFALL INTENSITY(INCH/HR) = 5.34  
TOTAL STREAM AREA(ACRES) = 2.67  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.69

\*\*\*\*\*  
FLOW PROCESS FROM NODE 180.00 TO NODE 181.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
-----  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
UPSTREAM ELEVATION(FEET) = 643.00  
DOWNSTREAM ELEVATION(FEET) = 633.00  
ELEVATION DIFFERENCE(FEET) = 10.00  
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.07 TOTAL RUNOFF(CFS) = 0.26

\*\*\*\*\*  
FLOW PROCESS FROM NODE 181.00 TO NODE 182.00 IS CODE = 53  
-----  
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<  
-----  
ELEVATION DATA: UPSTREAM(FEET) = 633.00 DOWNSTREAM(FEET) = 500.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 857.00 CHANNEL SLOPE = 0.1552  
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION  
CHANNEL FLOW THRU SUBAREA(CFS) = 0.26  
FLOW VELOCITY(FEET/SEC) = 2.21 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)  
TRAVEL TIME(MIN.) = 6.47 Tc(MIN.) = 10.65  
LONGEST FLOWPATH FROM NODE 180.00 TO NODE 182.00 = 957.00 FEET.

\*\*\*\*\*

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FLOW PROCESS FROM NODE      181.00 TO NODE      182.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.801
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) =      3.50  SUBAREA RUNOFF(CFS) =      7.98
TOTAL AREA(ACRES) =      3.6   TOTAL RUNOFF(CFS) =      8.14
TC(MIN.) =  10.65

```

```

*****
FLOW PROCESS FROM NODE      183.00 TO NODE      182.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  3.801
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) =      1.00  SUBAREA RUNOFF(CFS) =      2.28
TOTAL AREA(ACRES) =      4.6   TOTAL RUNOFF(CFS) =     10.42
TC(MIN.) =  10.65

```

```

*****
FLOW PROCESS FROM NODE      182.00 TO NODE      177.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  495.00  DOWNSTREAM(FEET) =  479.00
FLOW LENGTH(FEET) =  160.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  7.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  16.01
ESTIMATED PIPE DIAMETER(INCH) =  18.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  10.42
PIPE TRAVEL TIME(MIN.) =  0.17  Tc(MIN.) =  10.82
LONGEST FLOWPATH FROM NODE      180.00 TO NODE      177.00 =  1117.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE      177.00 TO NODE      177.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS =  3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  3 ARE:
TIME OF CONCENTRATION(MIN.) =  10.82
RAINFALL INTENSITY(INCH/HR) =  3.76
TOTAL STREAM AREA(ACRES) =  4.57
PEAK FLOW RATE(CFS) AT CONFLUENCE =  10.42

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.36	7.92	4.600	4.00
2	10.69	6.29	5.337	2.67
3	10.42	10.82	3.764	4.57

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	28.16	6.29	5.337
2	31.21	7.92	4.600
3	29.71	10.82	3.764

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) =  31.21  Tc(MIN.) =  7.92
TOTAL AREA(ACRES) =  11.2
LONGEST FLOWPATH FROM NODE      170.00 TO NODE      177.00 =  1168.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE      177.00 TO NODE      187.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   479.00  DOWNSTREAM(FEET) =   425.00
FLOW LENGTH(FEET) =   570.00  MANNING'S N =   0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   20.65
ESTIMATED PIPE DIAMETER(INCH) =   21.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =   31.21
PIPE TRAVEL TIME(MIN.) =   0.46  Tc(MIN.) =   8.38
LONGEST FLOWPATH FROM NODE      170.00 TO NODE      187.00 =   1738.00 FEET.
*****
FLOW PROCESS FROM NODE      187.00 TO NODE      187.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) =   8.38
RAINFALL INTENSITY(INCH/HR) =   4.44
TOTAL STREAM AREA(ACRES) =   11.24
PEAK FLOW RATE(CFS) AT CONFLUENCE =   31.21
*****
FLOW PROCESS FROM NODE      185.00 TO NODE      186.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500
INITIAL SUBAREA FLOW-LENGTH(FEET) =   65.00
UPSTREAM ELEVATION(FEET) =   485.25
DOWNSTREAM ELEVATION(FEET) =   484.60
ELEVATION DIFFERENCE(FEET) =   0.65
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =   5.079
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
          THE MAXIMUM OVERLAND FLOW LENGTH =   65.00
          (Reference: Table 3-1B of Hydrology Manual)
          THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   6.129
SUBAREA RUNOFF(CFS) =   0.87
TOTAL AREA(ACRES) =   0.19  TOTAL RUNOFF(CFS) =   0.87
*****
FLOW PROCESS FROM NODE      186.00 TO NODE      187.00 IS CODE =  61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STANDARD CURB SECTION USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =   484.60  DOWNSTREAM ELEVATION(FEET) =   430.00
STREET LENGTH(FEET) =   524.00  CURB HEIGHT(INCHES) =   6.0
STREET HALFWIDTH(FEET) =   16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =   8.00
INSIDE STREET CROSSFALL(DECIMAL) =   0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =   0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) =   0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =   0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =   0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =   5.78
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =   0.25
HALFSTREET FLOOD WIDTH(FEET) =   6.15
AVERAGE FLOW VELOCITY(FEET/SEC.) =   5.82
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =   1.45
STREET FLOW TRAVEL TIME(MIN.) =   1.50  Tc(MIN.) =   6.58
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   5.187
*USER SPECIFIED(SUBAREA):
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500

```

AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
SUBAREA AREA(ACRES) = 2.51 SUBAREA RUNOFF(CFS) = 9.76  
TOTAL AREA(ACRES) = 2.7 PEAK FLOW RATE(CFS) = 10.50

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 8.28  
FLOW VELOCITY(FEET/SEC.) = 6.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.91  
LONGEST FLOWPATH FROM NODE 185.00 TO NODE 187.00 = 589.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 187.00 TO NODE 187.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	6.58
RAINFALL INTENSITY(INCH/HR) =	5.19
TOTAL STREAM AREA(ACRES) =	2.70
PEAK FLOW RATE(CFS) AT CONFLUENCE =	10.50

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	31.21	8.38	4.436	11.24
2	10.50	6.58	5.187	2.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	37.19	6.58	5.187
2	40.19	8.38	4.436

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 40.19 Tc(MIN.) = 8.38  
TOTAL AREA(ACRES) = 13.9  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 187.00 = 1738.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 187.00 TO NODE 192.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	425.00	DOWNSTREAM(FEET) =	418.00
FLOW LENGTH(FEET) =	575.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS	23.0	INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.94		
ESTIMATED PIPE DIAMETER(INCH) =	30.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	40.19		
PIPE TRAVEL TIME(MIN.) =	0.96	Tc(MIN.) =	9.35
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 192.00 =	2313.00	FEET.	

\*\*\*\*\*  
FLOW PROCESS FROM NODE 192.00 TO NODE 192.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.35
RAINFALL INTENSITY(INCH/HR) =	4.14
TOTAL STREAM AREA(ACRES) =	13.94
PEAK FLOW RATE(CFS) AT CONFLUENCE =	40.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 190.00 TO NODE 191.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 434.55  
 DOWNSTREAM ELEVATION(FEET) = 433.90  
 ELEVATION DIFFERENCE(FEET) = 0.65  
 URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.079  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
 THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
 (Reference: Table 3-1B of Hydrology Manual)  
 THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.129  
 SUBAREA RUNOFF(CFS) = 0.37  
 TOTAL AREA(ACRES) = 0.08 TOTAL RUNOFF(CFS) = 0.37

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 191.00 TO NODE 192.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 433.90 DOWNSTREAM ELEVATION(FEET) = 423.00  
 STREET LENGTH(FEET) = 681.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 16.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 8.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.84  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.35  
 HALFSTREET FLOOD WIDTH(FEET) = 10.97  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.97  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.03  
 STREET FLOW TRAVEL TIME(MIN.) = 3.82 Tc(MIN.) = 8.90  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.268  
 \*USER SPECIFIED(SUBAREA):  
 DENSE RESIDENTIAL (R2,R3) RUNOFF COEFFICIENT = .7500  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.750  
 SUBAREA AREA(ACRES) = 4.57 SUBAREA RUNOFF(CFS) = 14.63  
 TOTAL AREA(ACRES) = 4.7 PEAK FLOW RATE(CFS) = 14.88

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 14.22  
 FLOW VELOCITY(FEET/SEC.) = 3.48 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.43  
 LONGEST FLOWPATH FROM NODE 190.00 TO NODE 192.00 = 746.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 192.00 TO NODE 192.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.90  
 RAINFALL INTENSITY(INCH/HR) = 4.27  
 TOTAL STREAM AREA(ACRES) = 4.65  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.88

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	40.19	9.35	4.135	13.94
2	14.88	8.90	4.268	4.65

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	40.19	9.35	4.135
2	14.88	8.90	4.268

1 53.83 8.90 4.268  
2 54.61 9.35 4.135

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 54.61 Tc(MIN.) = 9.35  
TOTAL AREA(ACRES) = 18.6  
LONGEST FLOWPATH FROM NODE 170.00 TO NODE 192.00 = 2313.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 192.00 TO NODE 162.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) =	418.00	DOWNSTREAM(FEET) =	362.00
FLOW LENGTH(FEET) =	539.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	24.0 INCH PIPE IS	16.1 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	24.40		
ESTIMATED PIPE DIAMETER(INCH) =	24.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	54.61		
PIPE TRAVEL TIME(MIN.) =	0.37	Tc(MIN.) =	9.72
LONGEST FLOWPATH FROM NODE	170.00 TO NODE	162.00 =	2852.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	54.61	9.72	4.034	18.59

LONGEST FLOWPATH FROM NODE 170.00 TO NODE 162.00 = 2852.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	130.04	10.02	3.955	42.97

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 162.00 = 3436.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	180.73	9.72	4.034
2	183.59	10.02	3.955

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 183.59 Tc(MIN.) = 10.02  
TOTAL AREA(ACRES) = 61.6

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 162.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 162.00 TO NODE 197.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) =	362.00	DOWNSTREAM(FEET) =	315.00
FLOW LENGTH(FEET) =	915.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	42.0 INCH PIPE IS	29.7 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	25.23		
ESTIMATED PIPE DIAMETER(INCH) =	42.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	183.59		
PIPE TRAVEL TIME(MIN.) =	0.60	Tc(MIN.) =	10.62
LONGEST FLOWPATH FROM NODE	110.00 TO NODE	197.00 =	4351.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.62
RAINFALL INTENSITY(INCH/HR) = 3.81
TOTAL STREAM AREA(ACRES) = 61.56
PEAK FLOW RATE(CFS) AT CONFLUENCE = 183.59

*****
FLOW PROCESS FROM NODE 195.00 TO NODE 196.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .7300
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 370.00
DOWNSTREAM ELEVATION(FEET) = 360.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.092
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.67
TOTAL AREA(ACRES) = 0.37 TOTAL RUNOFF(CFS) = 1.67

*****
FLOW PROCESS FROM NODE 196.00 TO NODE 197.00 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 360.60 DOWNSTREAM ELEVATION(FEET) = 318.50
STREET LENGTH(FEET) = 805.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 22.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.79
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.33
HALFSTREET FLOOD WIDTH(FEET) = 10.11
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.17
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.70
STREET FLOW TRAVEL TIME(MIN.) = 2.59 Tc(MIN.) = 5.69
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.699
*USER SPECIFIED(SUBAREA):
PAVED SURFACE RUNOFF COEFFICIENT = .7200
AREA-AVERAGE RUNOFF COEFFICIENT = 0.721
SUBAREA AREA(ACRES) = 4.90 SUBAREA RUNOFF(CFS) = 20.11
TOTAL AREA(ACRES) = 5.3 PEAK FLOW RATE(CFS) = 21.64

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 12.99
FLOW VELOCITY(FEET/SEC.) = 5.99 DEPTH*VELOCITY(FT*FT/SEC.) = 2.31
LONGEST FLOWPATH FROM NODE 195.00 TO NODE 197.00 = 905.00 FEET.

*****
FLOW PROCESS FROM NODE 197.00 TO NODE 197.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.69
RAINFALL INTENSITY(INCH/HR) = 5.70
TOTAL STREAM AREA(ACRES) = 5.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.64

```



\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	183.59	10.62	3.808	61.56
2	21.64	5.69	5.699	5.27

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	119.90	5.69	5.699
2	198.05	10.62	3.808

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 198.05 Tc(MIN.) = 10.62  
TOTAL AREA(ACRES) = 66.8  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 197.00 = 4351.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----  
ELEVATION DATA: UPSTREAM(FEET) = 313.00 DOWNSTREAM(FEET) = 283.50  
FLOW LENGTH(FEET) = 858.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 45.0 INCH PIPE IS 34.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.88  
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 198.05  
PIPE TRAVEL TIME(MIN.) = 0.65 Tc(MIN.) = 11.28  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 198.00 = 5209.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 197.00 TO NODE 198.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
-----  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.664  
\*USER SPECIFIED(SUBAREA):  
VEGETATED SLOPES (HILLY) RUNOFF COEFFICIENT = .5000  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.7261  
SUBAREA AREA(ACRES) = 2.15 SUBAREA RUNOFF(CFS) = 3.94  
TOTAL AREA(ACRES) = 69.0 TOTAL RUNOFF(CFS) = 198.05  
TC(MIN.) = 11.28  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*  
FLOW PROCESS FROM NODE 198.00 TO NODE 198.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<  
-----  
USER-SPECIFIED VALUES ARE AS FOLLOWS:  
TC(MIN) = 22.24 RAIN INTENSITY(INCH/HOUR) = 2.36  
TOTAL AREA(ACRES) = 68.98 TOTAL RUNOFF(CFS) = 98.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 198.00 TO NODE 304.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
-----  
ELEVATION DATA: UPSTREAM(FEET) = 278.00 DOWNSTREAM(FEET) = 200.00  
FLOW LENGTH(FEET) = 1006.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 30.0 INCH PIPE IS 22.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.02  
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 98.81  
PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 22.91  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 304.00 = 6215.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 22.91
RAINFALL INTENSITY(INCH/HR) = 2.32
TOTAL STREAM AREA(ACRES) = 68.98
PEAK FLOW RATE(CFS) AT CONFLUENCE = 98.81

*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 655.00
DOWNSTREAM ELEVATION(FEET) = 645.00
ELEVATION DIFFERENCE(FEET) = 10.00
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.178
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.192
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.23
TOTAL AREA(ACRES) = 0.33 TOTAL RUNOFF(CFS) = 1.23

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 53
-----
>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 645.00 DOWNSTREAM(FEET) = 450.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1066.00 CHANNEL SLOPE = 0.1829
CHANNEL FLOW THRU SUBAREA(CFS) = 1.23
FLOW VELOCITY(FEET/SEC) = 2.56 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 6.93 Tc(MIN.) = 11.11
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1166.00 FEET.

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.700
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 18.82 SUBAREA RUNOFF(CFS) = 41.78
TOTAL AREA(ACRES) = 19.1 TOTAL RUNOFF(CFS) = 42.51
TC(MIN.) = 11.11

*****
FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 305.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 2180.00 CHANNEL SLOPE = 0.0665
CHANNEL FLOW THRU SUBAREA(CFS) = 42.51
FLOW VELOCITY(FEET/SEC) = 9.53 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.81 Tc(MIN.) = 14.92
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 3346.00 FEET.

*****
FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.059
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000

```

SUBAREA AREA(ACRES) = 34.79 SUBAREA RUNOFF(CFS) = 63.84  
TOTAL AREA(ACRES) = 53.9 TOTAL RUNOFF(CFS) = 98.99  
TC(MIN.) = 14.92

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 53  
-----

>>>>COMPUTE NATURAL MOUNTAIN CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	305.00	DOWNSTREAM(FEET) =	200.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	751.00	CHANNEL SLOPE =	0.1398
CHANNEL FLOW THRU SUBAREA(CFS) =	98.99		
FLOW VELOCITY(FEET/SEC) =	9.67	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	1.29	Tc(MIN.) =	16.22
LONGEST FLOWPATH FROM NODE	300.00 TO NODE	304.00 =	4097.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	2.899		
*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
AREA-AVERAGE RUNOFF COEFFICIENT =	0.6000		
SUBAREA AREA(ACRES) =	4.88	SUBAREA RUNOFF(CFS) =	8.49
TOTAL AREA(ACRES) =	58.8	TOTAL RUNOFF(CFS) =	102.30
TC(MIN.) =	16.22		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	16.22
RAINFALL INTENSITY(INCH/HR) =	2.90
TOTAL STREAM AREA(ACRES) =	58.82
PEAK FLOW RATE(CFS) AT CONFLUENCE =	102.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 310.00 TO NODE 311.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED(SUBAREA):			
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT =	.6000		
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00		
UPSTREAM ELEVATION(FEET) =	410.00		
DOWNSTREAM ELEVATION(FEET) =	400.00		
ELEVATION DIFFERENCE(FEET) =	10.00		
URBAN SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.178		
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!			
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.192		
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.			
SUBAREA RUNOFF(CFS) =	2.38		
TOTAL AREA(ACRES) =	0.64	TOTAL RUNOFF(CFS) =	2.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 52  
-----

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	400.00	DOWNSTREAM(FEET) =	264.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	2121.00	CHANNEL SLOPE =	0.0641
CHANNEL FLOW THRU SUBAREA(CFS) =	2.38		
FLOW VELOCITY(FEET/SEC) =	4.52	(PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)	
TRAVEL TIME(MIN.) =	7.82	Tc(MIN.) =	12.00
LONGEST FLOWPATH FROM NODE	310.00 TO NODE	312.00 =	2221.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 312.00 IS CODE = 81  
-----

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.521
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 28.42 SUBAREA RUNOFF(CFS) = 60.03
TOTAL AREA(ACRES) = 29.1 TOTAL RUNOFF(CFS) = 61.39
TC(MIN.) = 12.00
*****
FLOW PROCESS FROM NODE 312.00 TO NODE 313.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 224.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1340.00 CHANNEL SLOPE = 0.0299
CHANNEL FLOW THRU SUBAREA(CFS) = 61.39
FLOW VELOCITY(FEET/SEC) = 7.10 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.15 Tc(MIN.) = 15.14
LONGEST FLOWPATH FROM NODE 310.00 TO NODE 313.00 = 3561.00 FEET.
*****
FLOW PROCESS FROM NODE 312.00 TO NODE 313.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.030
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 27.10 SUBAREA RUNOFF(CFS) = 49.26
TOTAL AREA(ACRES) = 56.2 TOTAL RUNOFF(CFS) = 102.08
TC(MIN.) = 15.14
*****
FLOW PROCESS FROM NODE 313.00 TO NODE 304.00 IS CODE = 52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 224.00 DOWNSTREAM(FEET) = 200.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1435.00 CHANNEL SLOPE = 0.0167
CHANNEL FLOW THRU SUBAREA(CFS) = 102.08
FLOW VELOCITY(FEET/SEC) = 6.18 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 3.87 Tc(MIN.) = 19.02
LONGEST FLOWPATH FROM NODE 310.00 TO NODE 304.00 = 4996.00 FEET.
*****
FLOW PROCESS FROM NODE 313.00 TO NODE 304.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.616
*USER SPECIFIED(SUBAREA):
VEGETATED SLOPES (STEEP) RUNOFF COEFFICIENT = .6000
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6000
SUBAREA AREA(ACRES) = 19.13 SUBAREA RUNOFF(CFS) = 30.02
TOTAL AREA(ACRES) = 75.3 TOTAL RUNOFF(CFS) = 118.16
TC(MIN.) = 19.02
*****
FLOW PROCESS FROM NODE 304.00 TO NODE 304.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 19.02
RAINFALL INTENSITY(INCH/HR) = 2.62
TOTAL STREAM AREA(ACRES) = 75.29
PEAK FLOW RATE(CFS) AT CONFLUENCE = 118.16

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	98.81	22.91	2.320	68.98
2	102.30	16.22	2.899	58.82
3	118.16	19.02	2.616	75.29

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	273.01	16.22	2.899
2	292.50	19.02	2.616
3	285.46	22.91	2.320

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 292.50 Tc(MIN.) = 19.02  
TOTAL AREA(ACRES) = 203.1  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 304.00 = 6215.00 FEET.

=====  
END OF STUDY SUMMARY:  
TOTAL AREA(ACRES) = 203.1 TC(MIN.) = 19.02  
PEAK FLOW RATE(CFS) = 292.50  
=====

=====  
END OF RATIONAL METHOD ANALYSIS

## **CHAPTER 4**

# **DETENTION BASIN ANALYSIS**

Basin – Stage Information

Stage – Storage

Stage- Discharge

Stage -Area

Depth	Area (sf)
0	29865
1	32381
2	34956
3	37590
4	40282
5	43034
6	45844
7	48715
8	51343



Basin #1 Discharge

Discharge vs Elevation Table

Low orifice:	4.5 "	Top orifice:	8 "
Number:	3	Number:	0
Cg-low:	0.61	Cg-low:	0.61
Invert elev:	0.50 ft	Invert elev:	0.00 ft
Middle orifice:	3 "	Emergency inlet:	
number of orif:	0	Rim height:	5.25 ft
Cg-middle:	0.61	Area	16.00 sq ft
Invert elev:	3.50 ft	Circumference	16.00 ft

<--- 4' x 4'

h (ft)	H/D-low	H/D-mid	H/D-top	Qlow-orif (cfs)	Qlow-weir (cfs)	Qtot-low (cfs)	Qmid-orif (cfs)	Qmid-weir (cfs)	Qtot-med (cfs)	Qtop-orif (cfs)	Qtop-weir (cfs)	Qtot-top (cfs)	Qemerg (cfs)	Qtot (cfs)
0.0	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.1	0.00	0.00	0.15	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.2	0.00	0.00	0.30	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.3	0.00	0.00	0.45	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.4	0.00	0.00	0.60	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.5	0.00	0.00	0.75	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.6	0.27	0.00	0.90	0.000	0.060	0.060	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.060
0.7	0.53	0.00	1.05	0.181	0.223	0.223	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.223
0.8	0.80	0.00	1.20	0.544	0.462	0.462	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.462
0.9	1.07	0.00	1.35	0.748	0.744	0.744	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.744
1.0	1.33	0.00	1.50	0.907	1.035	0.907	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.907
1.1	1.60	0.00	1.65	1.042	1.305	1.042	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.042
1.2	1.87	0.00	1.80	1.161	1.528	1.161	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.161
1.3	2.13	0.00	1.95	1.269	1.687	1.269	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.269
1.4	2.40	0.00	2.10	1.369	1.778	1.369	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.369
1.5	2.67	0.00	2.25	1.462	1.812	1.462	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.462
1.6	2.93	0.00	2.40	1.549	1.820	1.549	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.549
1.7	3.20	0.00	2.55	1.632	1.855	1.632	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.632
1.8	3.47	0.00	2.70	1.711	1.994	1.711	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.711
1.9	3.73	0.00	2.85	1.786	2.346	1.786	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.786
2.0	4.00	0.00	3.00	1.858	3.050	1.858	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.858
2.1	4.27	0.00	3.15	1.928	4.282	1.928	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.928
2.2	4.53	0.00	3.30	1.995	6.257	1.995	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.995
2.3	4.80	0.00	3.45	2.060	9.231	2.060	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.060
2.4	5.07	0.00	3.60	2.123	13.508	2.123	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.123
2.5	5.33	0.00	3.75	2.184	19.439	2.184	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.184
2.6	5.60	0.00	3.90	2.243	27.430	2.243	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.243
2.7	5.87	0.00	4.05	2.301	37.940	2.301	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.301
2.8	6.13	0.00	4.20	2.357	51.490	2.357	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.357
2.9	6.40	0.00	4.35	2.413	68.660	2.413	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.413
3.0	6.67	0.00	4.50	2.467	90.099	2.467	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.467
3.1	6.93	0.00	4.65	2.519	116.525	2.519	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.519
3.2	7.20	0.00	4.80	2.571	148.726	2.571	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.571
3.3	7.47	0.00	4.95	2.622	187.568	2.622	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.622
3.4	7.73	0.00	5.10	2.671	233.997	2.671	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.671
3.5	8.00	0.00	5.25	2.720	289.039	2.720	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.720
3.6	8.27	0.40	5.40	2.768	353.808	2.768	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.768
3.7	8.53	0.80	5.55	2.815	429.507	2.815	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.815
3.8	8.80	1.20	5.70	2.862	517.431	2.862	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.862
3.9	9.07	1.60	5.85	2.907	618.972	2.907	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.907
4.0	9.33	2.00	6.00	2.952	735.619	2.952	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.952
4.1	9.60	2.40	6.15	2.996	868.966	2.996	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.996
4.2	9.87	2.80	6.30	3.040	1020.713	3.040	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.040
4.3	10.13	3.20	6.45	3.083	1192.669	3.083	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.083
4.4	10.40	3.60	6.60	3.125	1386.754	3.125	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.125
4.5	10.67	4.00	6.75	3.167	1605.007	3.167	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.167
4.6	10.93	4.40	6.90	3.208	1849.584	3.208	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.208
4.7	11.20	4.80	7.05	3.249	2122.766	3.249	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.249
4.8	11.47	5.20	7.20	3.289	2426.957	3.289	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.289
4.9	11.73	5.60	7.35	3.329	2764.694	3.329	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.329
5.0	12.00	6.00	7.50	3.368	3138.644	3.368	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.368
5.1	12.27	6.40	7.65	3.407	3551.611	3.407	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.407
5.2	12.53	6.80	7.80	3.446	4006.540	3.446	0.000	0.000	0.000	0.000	0.000	0.000	0.000	3.446
5.3	12.80	7.20	7.95	3.483	4506.518	3.483	0.000	0.000	0.000	0.000	0.000	0.000	0.555	4.038
5.4	13.07	7.60	8.10	3.521	5054.776	3.521	0.000	0.000	0.000	0.000	0.000	0.000	2.881	6.403
5.5	13.33	8.00	8.25	3.558	5654.697	3.558	0.000	0.000	0.000	0.000	0.000	0.000	6.200	9.758
5.6	13.60	8.40	8.40	3.595	6309.817	3.595	0.000	0.000	0.000	0.000	0.000	0.000	10.270	13.865
5.7	13.87	8.80	8.55	3.631	7023.827	3.631	0.000	0.000	0.000	0.000	0.000	0.000	14.973	18.604
5.8	14.13	9.20	8.70	3.667	7800.578	3.667	0.000	0.000	0.000	0.000	0.000	0.000	20.231	23.899
5.9	14.40	9.60	8.85	3.703	8644.084	3.703	0.000	0.000	0.000	0.000	0.000	0.000	25.993	29.696
6.0	14.67	10.00	9.00	3.738	9558.525	3.738	0.000	0.000	0.000	0.000	0.000	0.000	32.216	35.955
6.1	14.93	10.40	9.15	3.774	#####	3.774	0.000	0.000	0.000	0.000	0.000	0.000	38.870	42.643



Otay Ranch Village 4 South  
TM Drainage Study

## 50 YEAR DETENTION

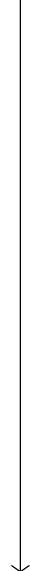
RUN DATE 6/22/2016  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 11 MIN.  
6 HOUR RAINFALL 2.13 INCHES  
BASIN AREA 68.98 ACRES  
RUNOFF COEFFICIENT 0.78  
PEAK DISCHARGE 178.35 CFS

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 11	DISCHARGE (CFS) = 6.8
TIME (MIN) = 22	DISCHARGE (CFS) = 7
TIME (MIN) = 33	DISCHARGE (CFS) = 7.3
TIME (MIN) = 44	DISCHARGE (CFS) = 7.4
TIME (MIN) = 55	DISCHARGE (CFS) = 7.8
TIME (MIN) = 66	DISCHARGE (CFS) = 8
TIME (MIN) = 77	DISCHARGE (CFS) = 8.4
TIME (MIN) = 88	DISCHARGE (CFS) = 8.7
TIME (MIN) = 99	DISCHARGE (CFS) = 9.2
TIME (MIN) = 110	DISCHARGE (CFS) = 9.5
TIME (MIN) = 121	DISCHARGE (CFS) = 10.2
TIME (MIN) = 132	DISCHARGE (CFS) = 10.6
TIME (MIN) = 143	DISCHARGE (CFS) = 11.5
TIME (MIN) = 154	DISCHARGE (CFS) = 12
TIME (MIN) = 165	DISCHARGE (CFS) = 13.3
TIME (MIN) = 176	DISCHARGE (CFS) = 14.2
TIME (MIN) = 187	DISCHARGE (CFS) = 16.2
TIME (MIN) = 198	DISCHARGE (CFS) = 17.6
TIME (MIN) = 209	DISCHARGE (CFS) = 21.5
TIME (MIN) = 220	DISCHARGE (CFS) = 24.5
TIME (MIN) = 231	DISCHARGE (CFS) = 36
TIME (MIN) = 242	DISCHARGE (CFS) = 53.9
TIME (MIN) = 253	DISCHARGE (CFS) = 178.35
TIME (MIN) = 264	DISCHARGE (CFS) = 28.8
TIME (MIN) = 275	DISCHARGE (CFS) = 19.3
TIME (MIN) = 286	DISCHARGE (CFS) = 15.1
TIME (MIN) = 297	DISCHARGE (CFS) = 12.6
TIME (MIN) = 308	DISCHARGE (CFS) = 11
TIME (MIN) = 319	DISCHARGE (CFS) = 9.8
TIME (MIN) = 330	DISCHARGE (CFS) = 8.9
TIME (MIN) = 341	DISCHARGE (CFS) = 8.2
TIME (MIN) = 352	DISCHARGE (CFS) = 7.6
TIME (MIN) = 363	DISCHARGE (CFS) = 7.1
TIME (MIN) = 374	DISCHARGE (CFS) = 0

<b>Watershed Model Schematic.....</b>	<b>1</b>
<b>50 - Year</b>	
<b>Summary Report.....</b>	<b>2</b>
<b>Hydrograph Reports.....</b>	<b>3</b>
Hydrograph No. 1, Manual, Village 4.....	3
Hydrograph No. 2, Reservoir, <no description>.....	4
Pond Report - BASIN 1.....	5

# Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3



## Legend

<u>Hyd. Origin</u>	<u>Description</u>
1	Manual Village 4
2	Reservoir <no description>

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	Manual	178.35	11	253	414,711	-----	-----	-----	Village 4	
2	Reservoir	83.92	11	264	414,676	1	289.03	256,500	<no description>	
V4 50yr detention 4 x 4 riser.gpw					Return Period: 50 Year			Wednesday, 06 / 22 / 2016		

# Hydrograph Report

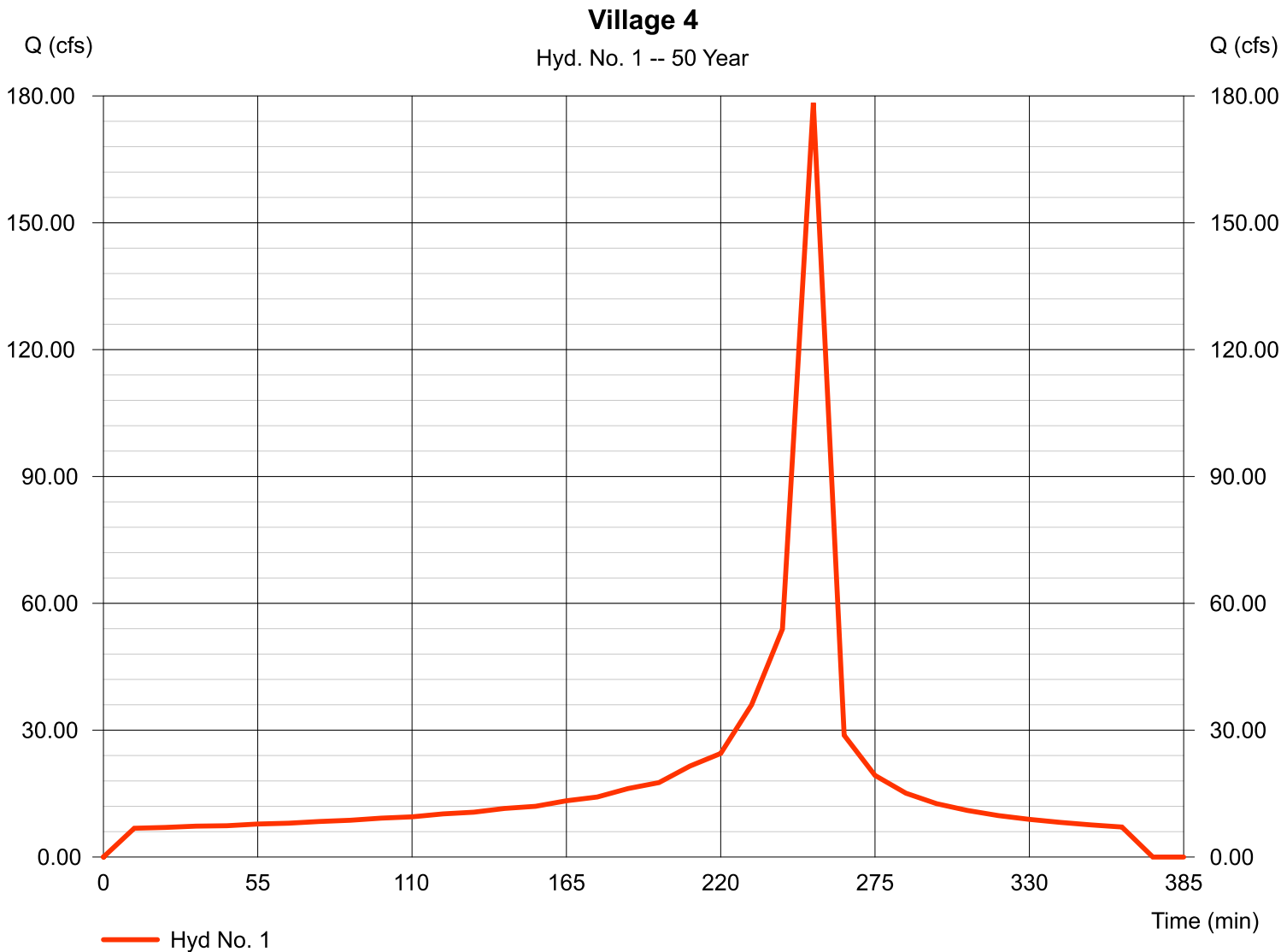
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Wednesday, 06 / 22 / 2016

## Hyd. No. 1

Village 4

Hydrograph type	= Manual	Peak discharge	= 178.35 cfs
Storm frequency	= 50 yrs	Time to peak	= 253 min
Time interval	= 11 min	Hyd. volume	= 414,711 cuft





# Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

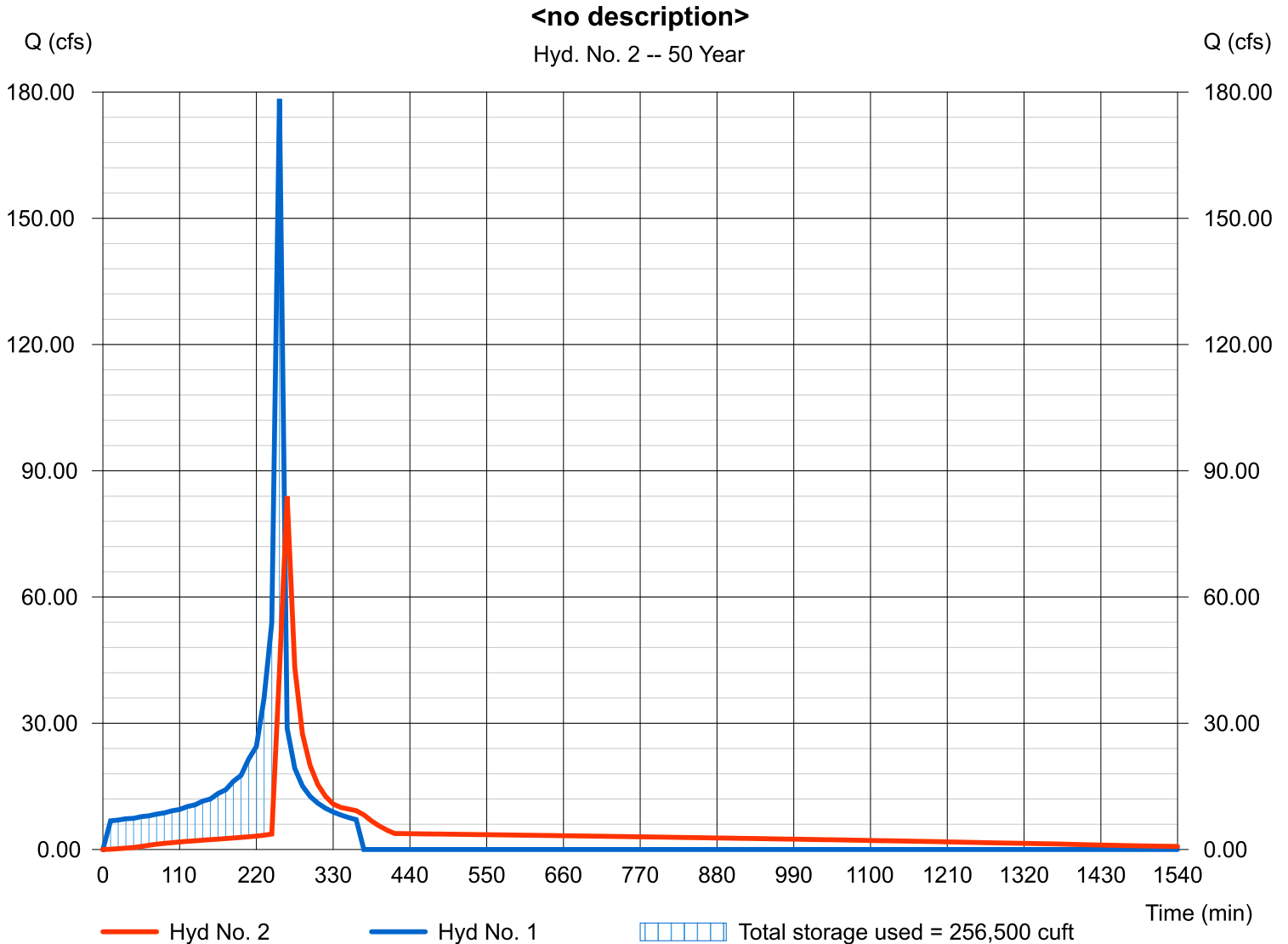
Wednesday, 06 / 22 / 2016

## Hyd. No. 2

<no description>

Hydrograph type	= Reservoir	Peak discharge	= 83.92 cfs
Storm frequency	= 50 yrs	Time to peak	= 264 min
Time interval	= 11 min	Hyd. volume	= 414,676 cuft
Inflow hyd. No.	= 1 - Village 4	Max. Elevation	= 289.03 ft
Reservoir name	= BASIN 1	Max. Storage	= 256,500 cuft

Storage Indication method used.



## Pond No. 1 - BASIN 1

### Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 282.00 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	282.00	29,865	0	0
0.50	282.50	31,116	15,245	15,245
1.00	283.00	32,381	15,874	31,120
1.50	283.50	33,661	16,511	47,630
2.00	284.00	34,956	17,154	64,784
2.50	284.50	36,265	17,805	82,590
3.00	285.00	37,589	18,464	101,053
3.50	285.50	38,928	19,129	120,182
4.00	286.00	40,282	19,803	139,985
4.50	286.50	41,651	20,483	160,468
5.00	287.00	43,034	21,171	181,639
5.50	287.50	44,432	21,867	203,506
6.00	288.00	45,844	22,569	226,075
6.50	288.50	47,272	23,279	249,354
7.00	289.00	48,715	23,997	273,351
7.50	289.50	50,172	24,722	298,072
8.00	290.00	51,643	25,454	323,526

### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0
Invert El. (ft)	= 0.00	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000	(by Contour)		
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

### Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Civ A cfs	Civ B cfs	Civ C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	282.00	---	---	---	---	---	---	---	---	---	---	0.000
0.50	15,245	282.50	---	---	---	---	---	---	---	---	---	0.432	0.432
1.00	31,120	283.00	---	---	---	---	---	---	---	---	---	1.338	1.338
1.50	47,630	283.50	---	---	---	---	---	---	---	---	---	1.894	1.894
2.00	64,784	284.00	---	---	---	---	---	---	---	---	---	2.290	2.290
2.50	82,590	284.50	---	---	---	---	---	---	---	---	---	2.615	2.615
3.00	101,053	285.00	---	---	---	---	---	---	---	---	---	2.898	2.898
3.50	120,182	285.50	---	---	---	---	---	---	---	---	---	3.152	3.152
4.00	139,985	286.00	---	---	---	---	---	---	---	---	---	3.384	3.384
4.50	160,468	286.50	---	---	---	---	---	---	---	---	---	3.599	3.599
5.00	181,639	287.00	---	---	---	---	---	---	---	---	---	3.800	3.800
5.50	203,506	287.50	---	---	---	---	---	---	---	---	---	10.19	10.19
6.00	226,075	288.00	---	---	---	---	---	---	---	---	---	36.39	36.39
6.50	249,354	288.50	---	---	---	---	---	---	---	---	---	73.66	73.66
7.00	273,351	289.00	---	---	---	---	---	---	---	---	---	108.12	108.12
7.50	298,072	289.50	---	---	---	---	---	---	---	---	---	122.15	122.15
8.00	323,526	290.00	---	---	---	---	---	---	---	---	---	134.70	134.70

Otay Ranch Village 4 South  
TM Drainage Study

## 100 YEAR DETENTION

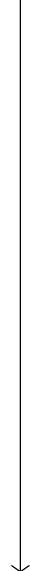
RUN DATE 6/22/2016  
HYDROGRAPH FILE NAME Text1  
TIME OF CONCENTRATION 11 MIN.  
6 HOUR RAINFALL 2.35 INCHES  
BASIN AREA 68.98 ACRES  
RUNOFF COEFFICIENT 0.78  
PEAK DISCHARGE 198.05 CFS

TIME (MIN) = 0	DISCHARGE (CFS) = 0
TIME (MIN) = 11	DISCHARGE (CFS) = 7.5
TIME (MIN) = 22	DISCHARGE (CFS) = 7.7
TIME (MIN) = 33	DISCHARGE (CFS) = 8
TIME (MIN) = 44	DISCHARGE (CFS) = 8.2
TIME (MIN) = 55	DISCHARGE (CFS) = 8.6
TIME (MIN) = 66	DISCHARGE (CFS) = 8.8
TIME (MIN) = 77	DISCHARGE (CFS) = 9.3
TIME (MIN) = 88	DISCHARGE (CFS) = 9.5
TIME (MIN) = 99	DISCHARGE (CFS) = 10.1
TIME (MIN) = 110	DISCHARGE (CFS) = 10.5
TIME (MIN) = 121	DISCHARGE (CFS) = 11.2
TIME (MIN) = 132	DISCHARGE (CFS) = 11.7
TIME (MIN) = 143	DISCHARGE (CFS) = 12.7
TIME (MIN) = 154	DISCHARGE (CFS) = 13.3
TIME (MIN) = 165	DISCHARGE (CFS) = 14.7
TIME (MIN) = 176	DISCHARGE (CFS) = 15.6
TIME (MIN) = 187	DISCHARGE (CFS) = 17.9
TIME (MIN) = 198	DISCHARGE (CFS) = 19.4
TIME (MIN) = 209	DISCHARGE (CFS) = 23.7
TIME (MIN) = 220	DISCHARGE (CFS) = 27
TIME (MIN) = 231	DISCHARGE (CFS) = 39.7
TIME (MIN) = 242	DISCHARGE (CFS) = 58.2
TIME (MIN) = 253	DISCHARGE (CFS) = 198.05
TIME (MIN) = 264	DISCHARGE (CFS) = 31.8
TIME (MIN) = 275	DISCHARGE (CFS) = 21.3
TIME (MIN) = 286	DISCHARGE (CFS) = 16.7
TIME (MIN) = 297	DISCHARGE (CFS) = 14
TIME (MIN) = 308	DISCHARGE (CFS) = 12.1
TIME (MIN) = 319	DISCHARGE (CFS) = 10.8
TIME (MIN) = 330	DISCHARGE (CFS) = 9.8
TIME (MIN) = 341	DISCHARGE (CFS) = 9
TIME (MIN) = 352	DISCHARGE (CFS) = 8.4
TIME (MIN) = 363	DISCHARGE (CFS) = 7.8
TIME (MIN) = 374	DISCHARGE (CFS) = 0

<b>Watershed Model Schematic.....</b>	<b>1</b>
<b>100 - Year</b>	
<b>Summary Report.....</b>	<b>2</b>
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Hydrograph No. 2, Reservoir, <no description>.....	3
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# Watershed Model Schematic

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3



## Legend

<u>Hyd. Origin</u>	<u>Description</u>
1	Manual Village 4
2	Reservoir <no description>

# Hydrograph Summary Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	Manual	198.05	11	253	457,413	-----	-----	-----	Village 4	
2	Reservoir	98.71	11	264	457,378	1	289.31	266,796	<no description>	
V4 100yr detention 4 x 4 riser.gpw					Return Period: 100 Year			Wednesday, 06 / 22 / 2016		

# Hydrograph Report

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2014 by Autodesk, Inc. v10.3

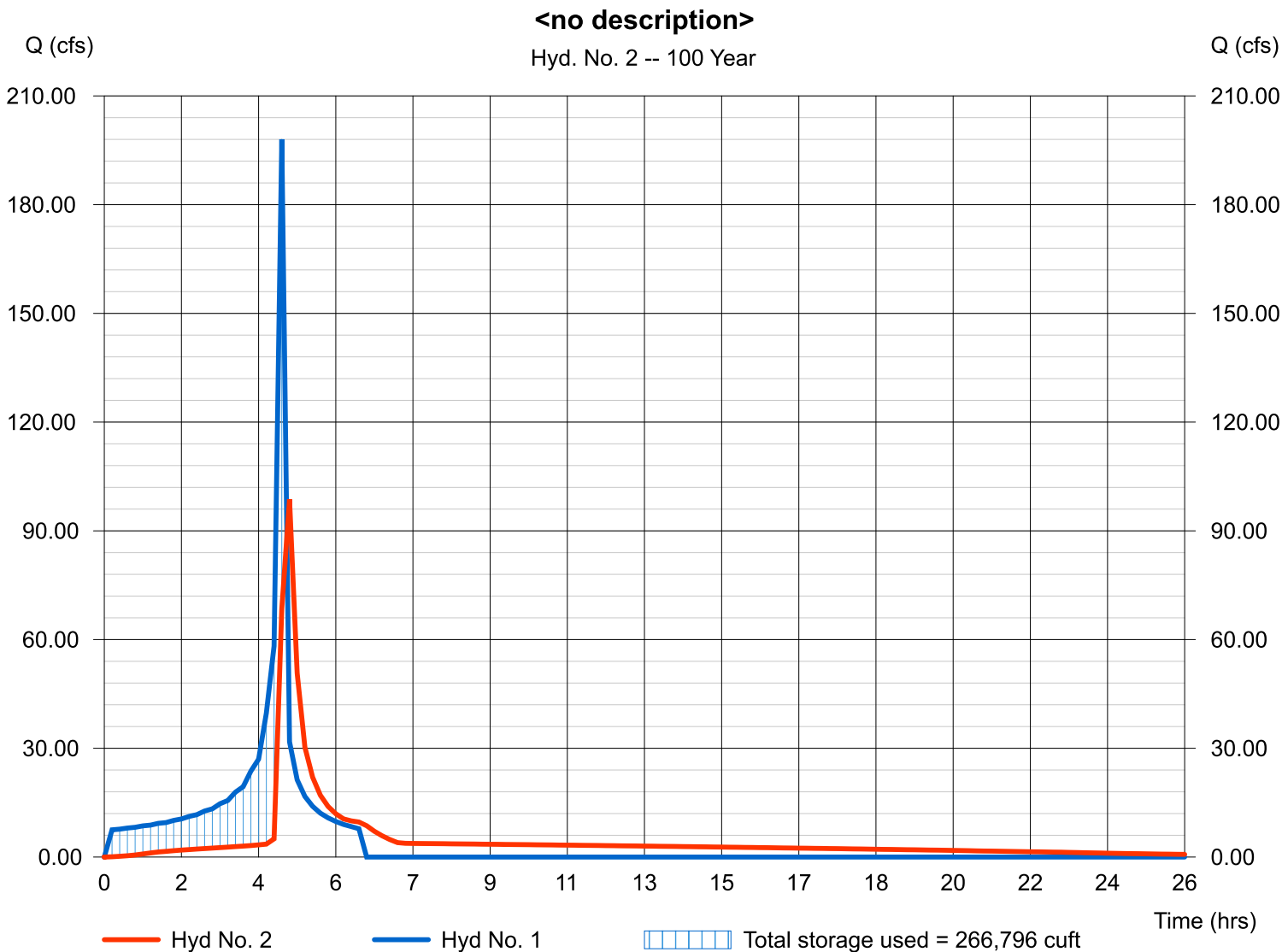
Wednesday, 06 / 22 / 2016

## Hyd. No. 2

<no description>

Hydrograph type	= Reservoir	Peak discharge	= 98.71 cfs
Storm frequency	= 100 yrs	Time to peak	= 4.40 hrs
Time interval	= 11 min	Hyd. volume	= 457,378 cuft
Inflow hyd. No.	= 1 - Village 4	Max. Elevation	= 289.31 ft
Reservoir name	= BASIN 1	Max. Storage	= 266,796 cuft

Storage Indication method used.





## Pond No. 1 - BASIN 1

### Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 282.00 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	282.00	29,865	0	0
0.50	282.50	31,116	15,245	15,245
1.00	283.00	32,381	15,874	31,120
1.50	283.50	33,661	16,511	47,630
2.00	284.00	34,956	17,154	64,784
2.50	284.50	36,265	17,805	82,590
3.00	285.00	37,589	18,464	101,053
3.50	285.50	38,928	19,129	120,182
4.00	286.00	40,282	19,803	139,985
4.50	286.50	41,651	20,483	160,468
5.00	287.00	43,034	21,171	181,639
5.50	287.50	44,432	21,867	203,506
6.00	288.00	45,844	22,569	226,075
6.50	288.50	47,272	23,279	249,354
7.00	289.00	48,715	23,997	273,351
7.50	289.50	50,172	24,722	298,072
8.00	290.00	51,643	25,454	323,526

### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 0.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00
No. Barrels	= 0	0	0	0
Invert El. (ft)	= 0.00	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 0.00	0.00	0.00	0.00
Crest El. (ft)	= 0.00	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= ---	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000	(by Contour)		
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

### Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Civ A cfs	Civ B cfs	Civ C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	282.00	---	---	---	---	---	---	---	---	---	---	0.000
0.50	15,245	282.50	---	---	---	---	---	---	---	---	---	0.432	0.432
1.00	31,120	283.00	---	---	---	---	---	---	---	---	---	1.338	1.338
1.50	47,630	283.50	---	---	---	---	---	---	---	---	---	1.894	1.894
2.00	64,784	284.00	---	---	---	---	---	---	---	---	---	2.290	2.290
2.50	82,590	284.50	---	---	---	---	---	---	---	---	---	2.615	2.615
3.00	101,053	285.00	---	---	---	---	---	---	---	---	---	2.898	2.898
3.50	120,182	285.50	---	---	---	---	---	---	---	---	---	3.152	3.152
4.00	139,985	286.00	---	---	---	---	---	---	---	---	---	3.384	3.384
4.50	160,468	286.50	---	---	---	---	---	---	---	---	---	3.599	3.599
5.00	181,639	287.00	---	---	---	---	---	---	---	---	---	3.800	3.800
5.50	203,506	287.50	---	---	---	---	---	---	---	---	---	10.19	10.19
6.00	226,075	288.00	---	---	---	---	---	---	---	---	---	36.39	36.39
6.50	249,354	288.50	---	---	---	---	---	---	---	---	---	73.66	73.66
7.00	273,351	289.00	---	---	---	---	---	---	---	---	---	108.12	108.12
7.50	298,072	289.50	---	---	---	---	---	---	---	---	---	122.15	122.15
8.00	323,526	290.00	---	---	---	---	---	---	---	---	---	134.70	134.70

## BASIN DRAWDOWN CALCULTIONS

# Village 4 Basin Drawdown Calculations using HEC HMS

The screenshot displays the HEC HMS software interface. The main window is titled "Basin Model [V4 Detention] Current Run [Run 1]". A smaller window titled "Summary Results for Reservoir 'V4 detention'" is open in the foreground, displaying the following information:

Project: Village 4  
Simulation Run: Run 1 Reservoir: V4 detention

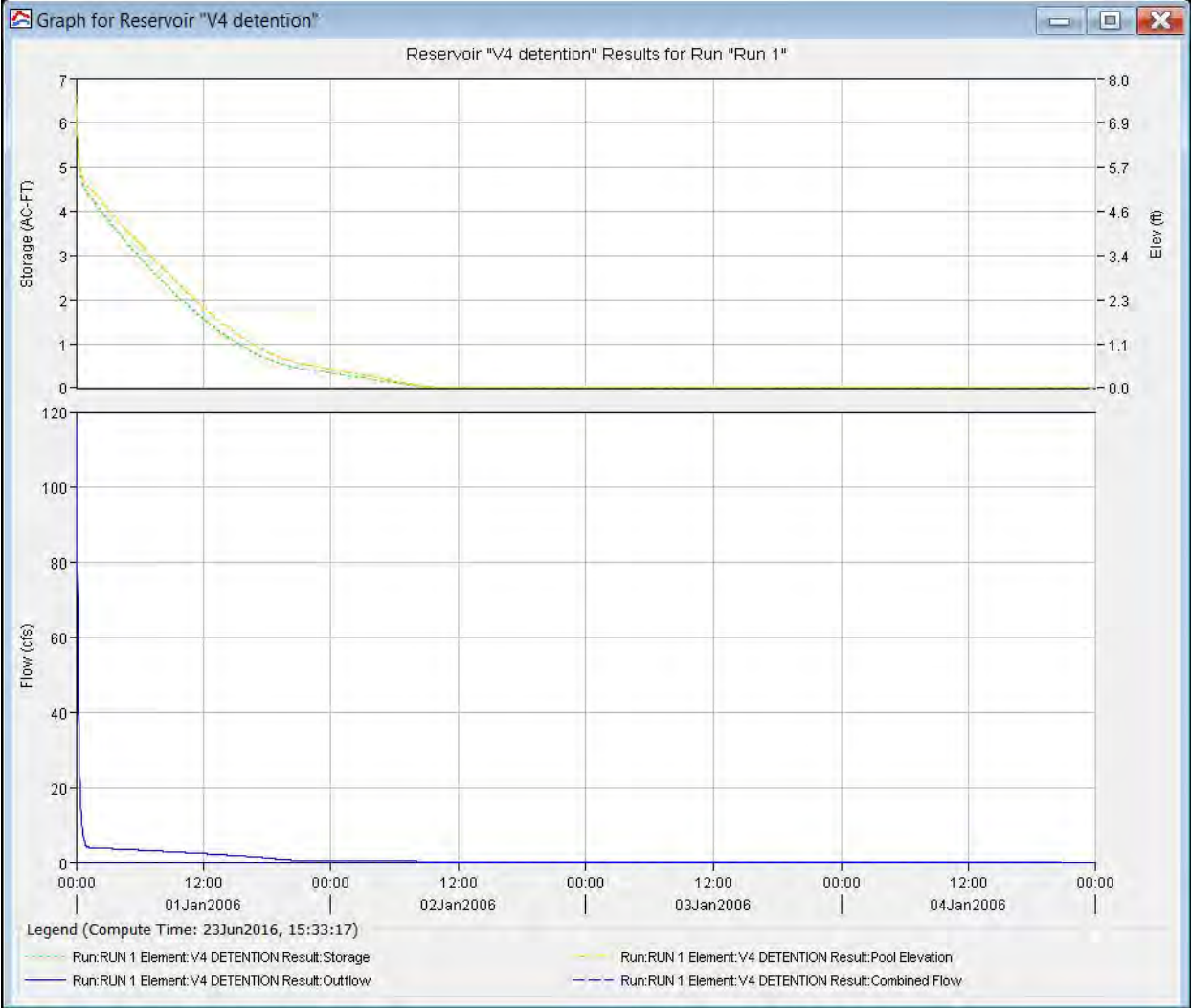
Start of Run: 01Jan2006, 00:00	Basin Model: V4 Detention
End of Run: 05Jan2006, 00:00	Meteorologic Model: NONE
Compute Time: 23Jun2016, 15:33:17	Control Specifications: 24-96 HRS

Volume Units:  IN  AC-FT

Computed Results

Peak Inflow : 0.0 (CFS)	Date/Time of Peak Inflow : 01Jan2006, 00:00
Peak Outflow : 117.0 (CFS)	Date/Time of Peak Outflow : 01Jan2006, 00:00
Total Inflow : (IN)	Peak Storage : 6.6 (AC-FT)
Total Outflow : (IN)	Peak Elevation : 7.3 (FT)

Below the summary window, there is a small icon labeled "V4 detention" on a grid background.



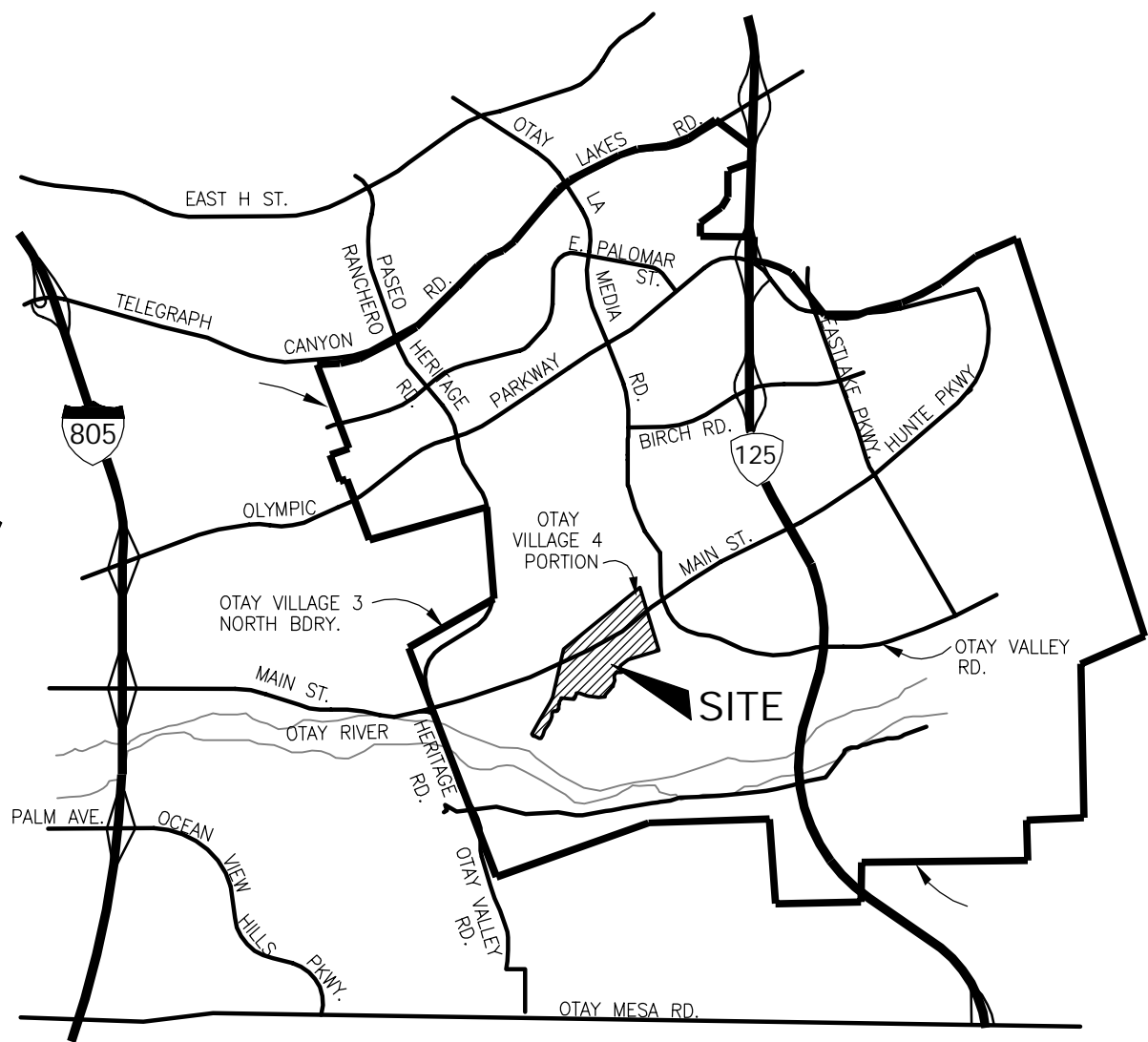
## **CHAPTER 5**

### **EXHIBIT 1 PRE-DEVELOPED CONDITION HYDROLOGY MAP**

### **EXHIBIT 2 DEVELOPED CONDITION HYDROLOGY MAP**

### **EXHIBIT 3 OVERLAY OF FLOOD INSURANCE RATE MAP**



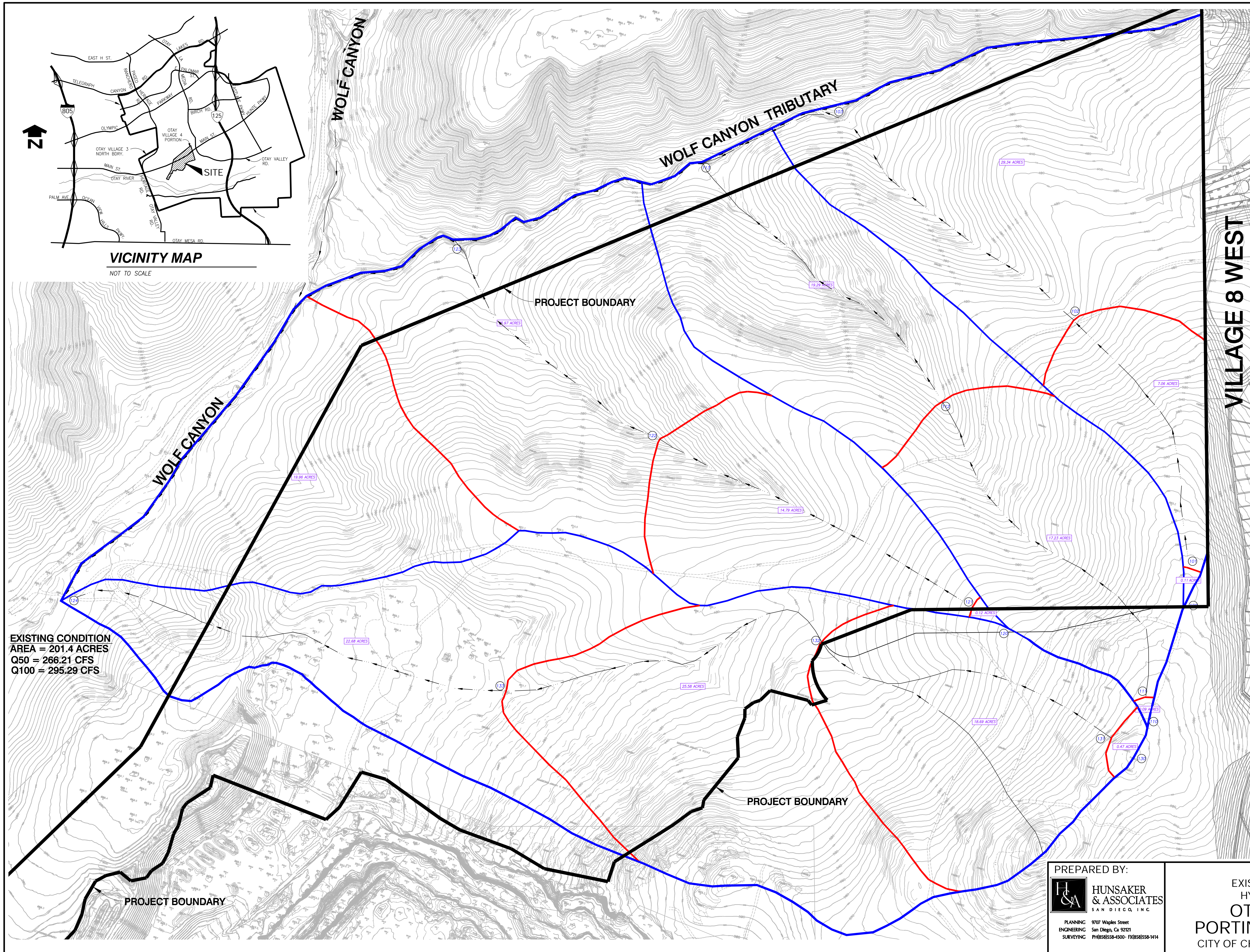


**VICINITY MAP**

NOT TO SCALE

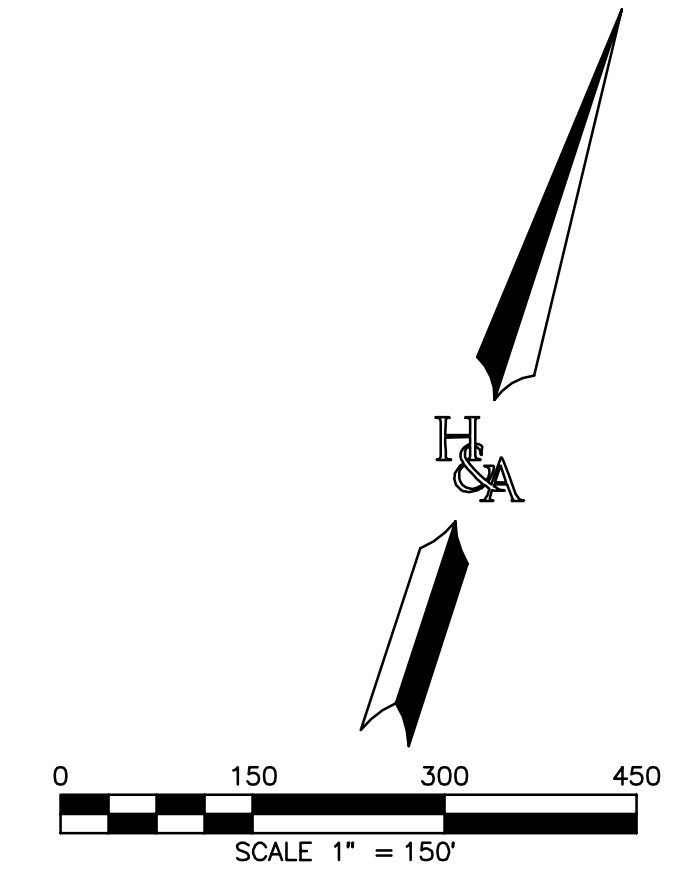
# LEGEND

- PROJECT BOUNDARY
- DRAINAGE BOUNDARY
- INITIAL SUBAREA
- FLOW DIRECTION
- NODE #
- SUBAREA ACREAGE



EXISTING CONDITION  
AREA = 201.4 ACRES  
Q50 = 266.21 CFS  
Q100 = 295.29 CFS

VILLAGE 8 WEST

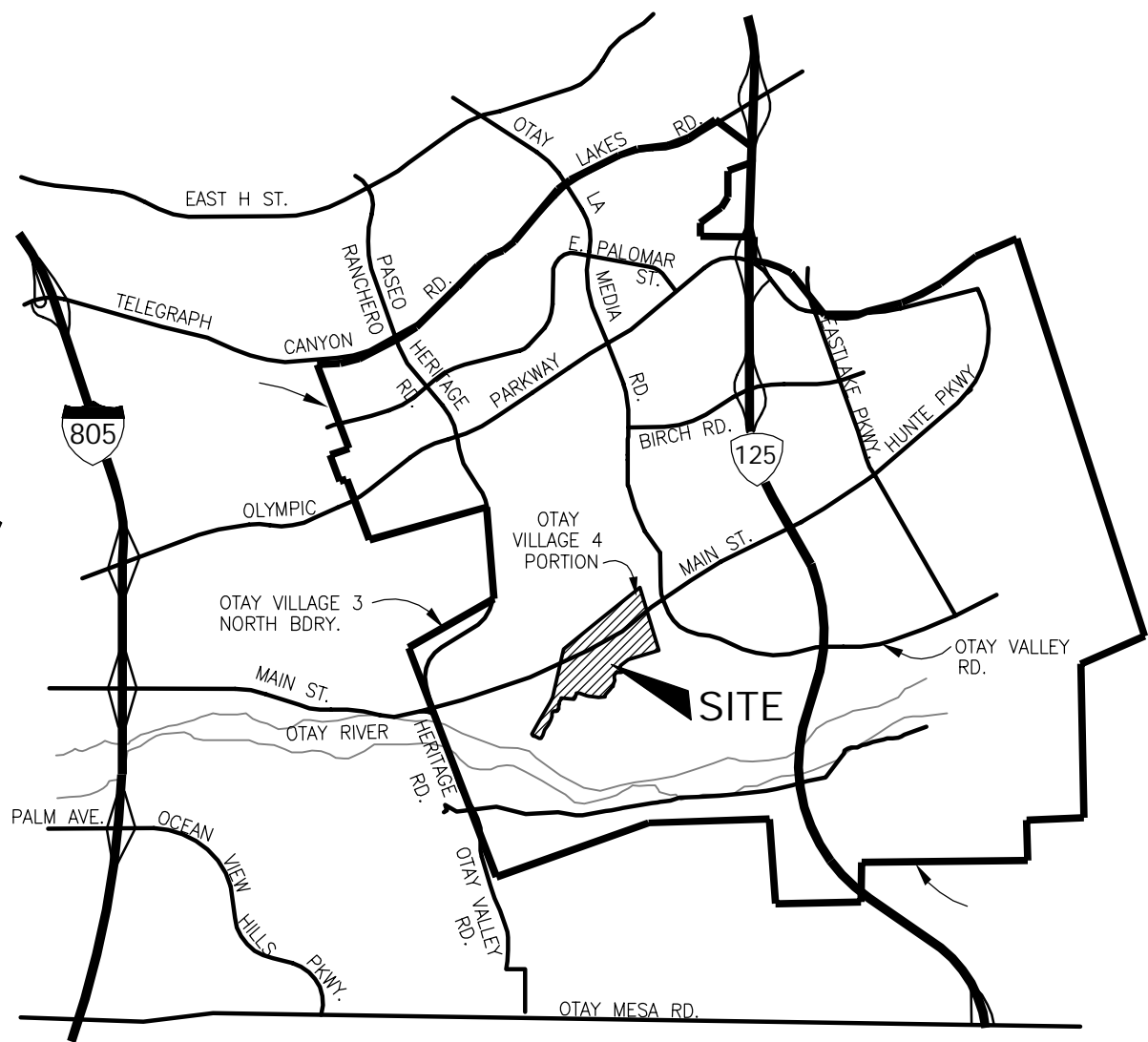


PREPARED BY:  
**HUNSAKER & ASSOCIATES**  
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 PLANNING 9707 Waples Street  
 ENGINEERING San Diego, Ca 92121  
 SURVEYING PH(619)558-4500 FX(619)558-1414

EXHIBIT 1  
 EXISTING CONDITION  
 HYDROLOGY MAP  
**OTAY RANCH**  
 PORTIN OF VILLAGE 4  
 CITY OF CHULA VISTA, CALIFORNIA

MAP  
 1  
 OF  
 2



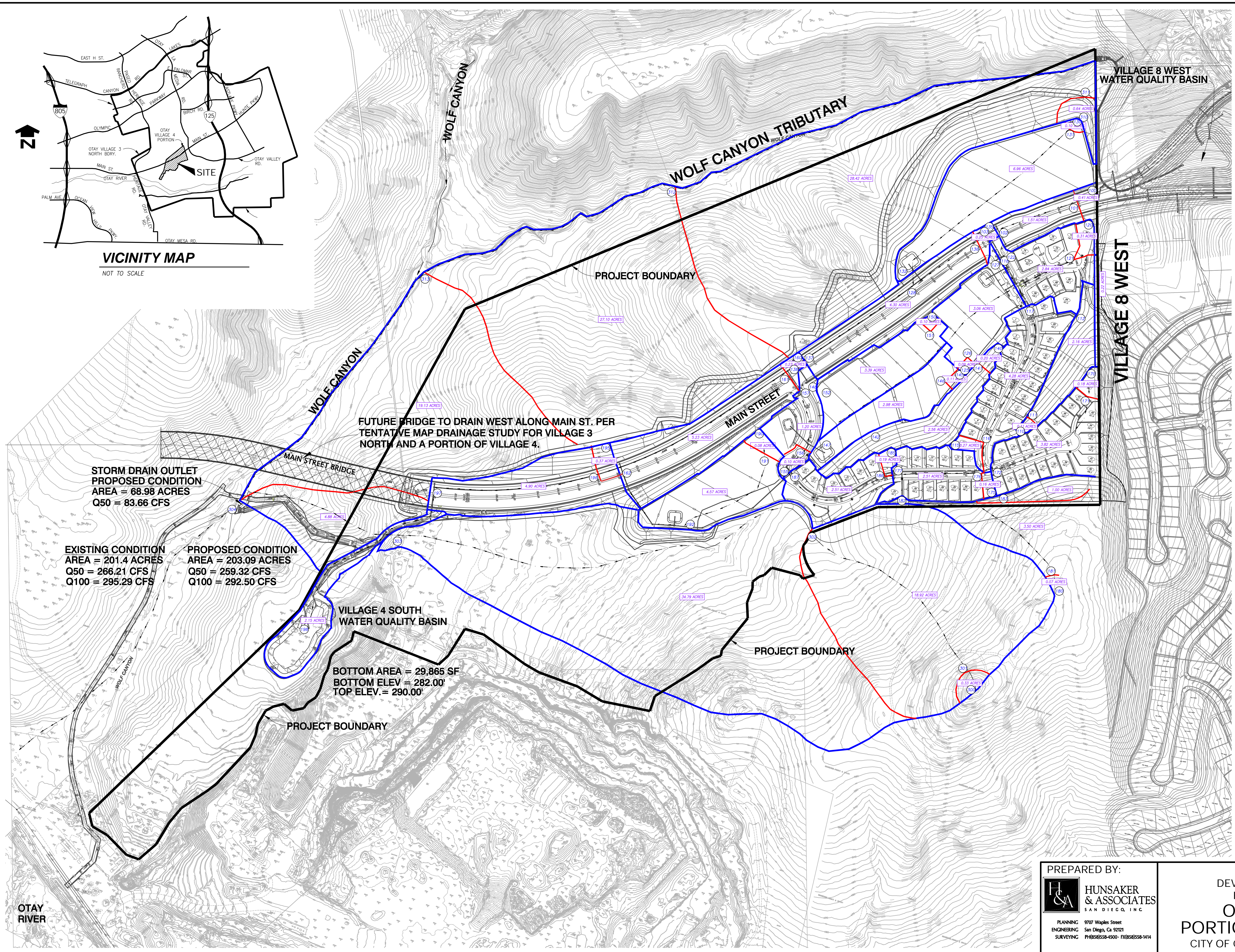


**VICINITY MAP**

NOT TO SCALE

# LEGEND

- PROJECT BOUNDARY
- DRAINAGE BOUNDARY
- INITIAL SUBAREA
- FLOW DIRECTION
- NODE #
- SUBAREA ACREAGE



FUTURE BRIDGE TO DRAIN WEST ALONG MAIN ST. PER TENTATIVE MAP DRAINAGE STUDY FOR VILLAGE 3 NORTH AND A PORTION OF VILLAGE 4.

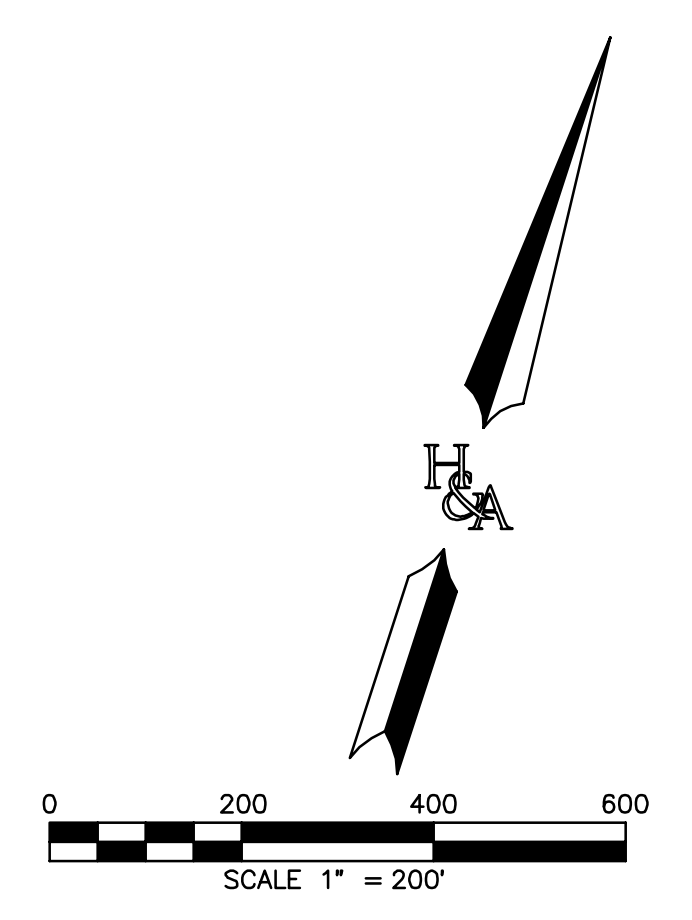
STORM DRAIN OUTLET  
PROPOSED CONDITION  
AREA = 68.98 ACRES  
Q50 = 83.66 CFS

EXISTING CONDITION  
AREA = 201.4 ACRES  
Q50 = 266.21 CFS  
Q100 = 295.29 CFS

PROPOSED CONDITION  
AREA = 203.09 ACRES  
Q50 = 259.32 CFS  
Q100 = 292.50 CFS

VILLAGE 4 SOUTH  
WATER QUALITY BASIN

BOTTOM AREA = 29,865 SF  
BOTTOM ELEV = 282.00'  
TOP ELEV. = 290.00'

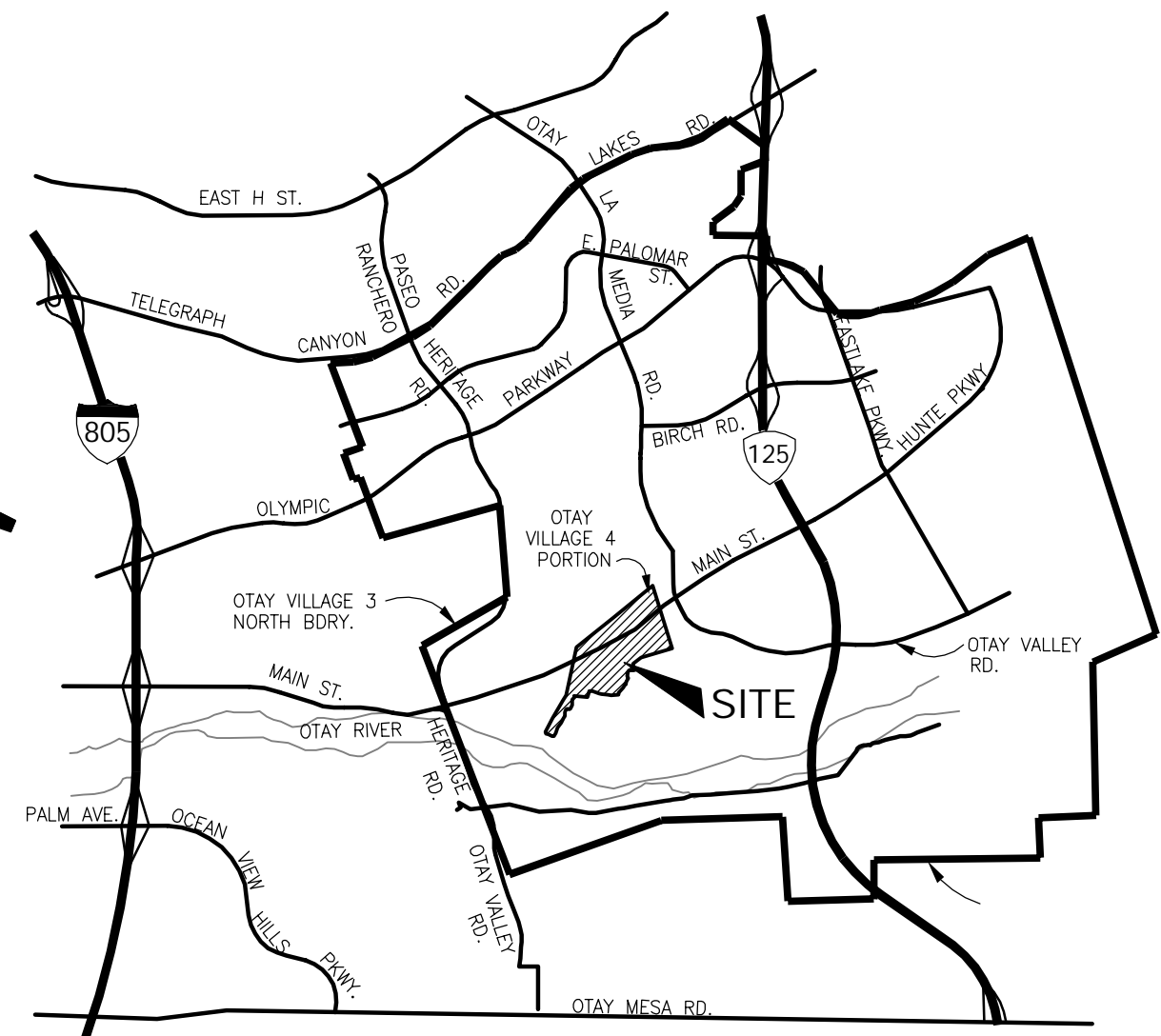


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EXHIBIT 2  
 DEVELOPED CONDITION  
 HYDROLOGY MAP  
**OTAY RANCH**  
 PORTION OF VILLAGE 4  
 CITY OF CHULA VISTA, CALIFORNIA

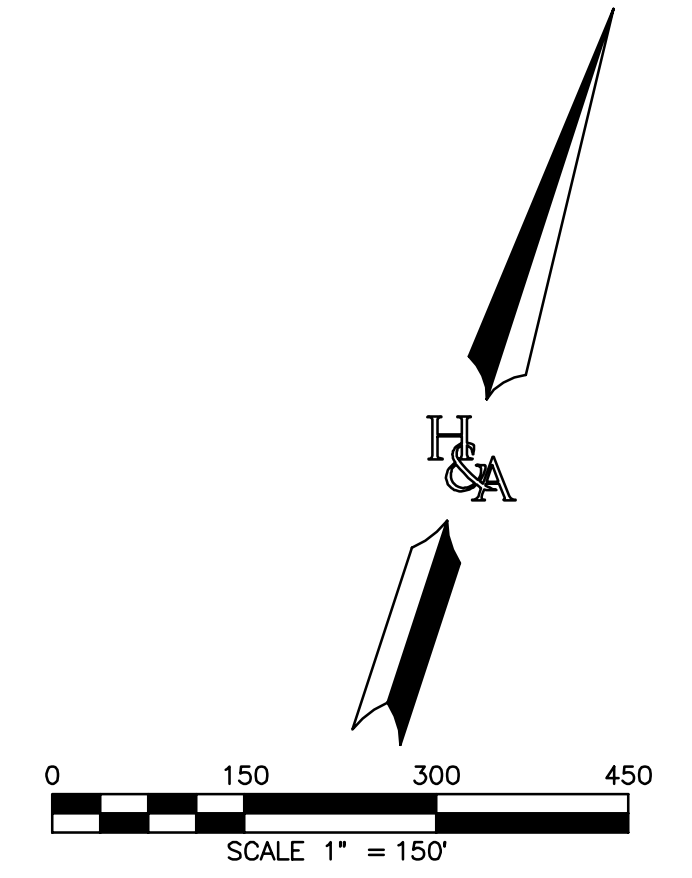
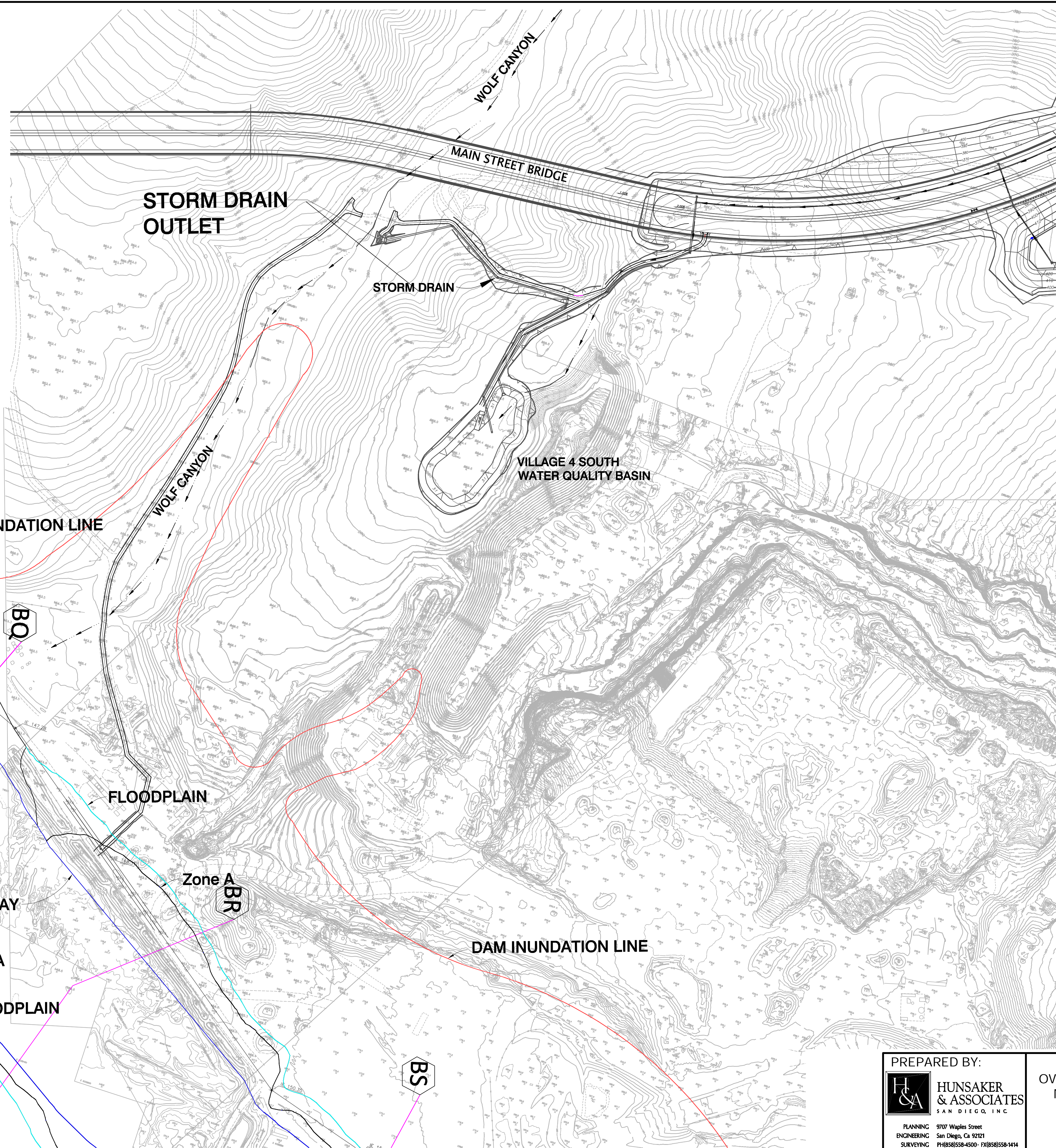
MAP  
 2  
 OF  
 3





VICINITY MAP

NOT TO SCALE



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 **HUNSAKER & ASSOCIATES**  
 SAN DIEGO, INC.  
 PLANNING: 9707 Waples Street  
 ENGINEERING: San Diego, Ca 92121  
 SURVEYING: PH(619)558-4500 FX(619)558-1414

EXHIBIT 3  
 OVERLAY OF FLOOD INSURANCE RATE MAP  
 NOS. 06073C2178G AND 06073C2176G  
**OTAY RANCH**  
**VILLAGE 4 SOUTH**  
 CITY OF CHULA VISTA, CALIFORNIA

MAP  
**3**  
 OF  
**3**